

A sharp cartesian method for the simulation of air-water interface

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Numerical Analysis Seminar
Texas A&M University
Sept. 11th, 2014

Motivation: sharp simulation of air-water interface

- Starting point:
 - NaSCar: a 3D parallel incompressible code with fluid-solid interaction
 - a second order cartesian method to solve elliptic problems with discontinuities across interfaces
- ⇒adaptation of this method to solve accurately the pressure at the interface between fluids with strong density ratios
- Our aim: simulation of solids interacting with fluids with strong density ratios (air-water interface)
 - wave breaking
 - marine engineering
 - wave energy converters



Bibliography

Only few sharp methods on cartesian grids in this context:

- Kang, Fedkiw and Liu 2000:
application of the famous "Ghost Fluid Method",
pioneering work, but non-physical effects due to poor momentum
preservation for each fluid
- Raessi and Pitsch 2012: "cut-cell"-like method
- Zhou et al 2012: only for fixed interface

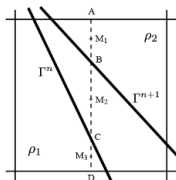
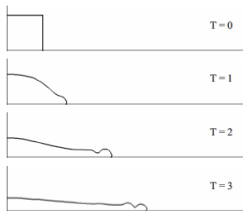
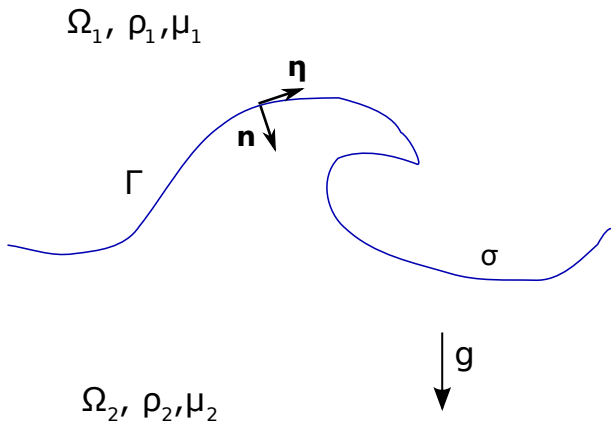


Figure 3: The phase interface Γ at time steps n and $n+1$ intersecting with a flux surface (dashed line).

Figure: Left: non physical behavior for dam-break problem (Kang et. al.), right: "cut-cell" interface reconstruction (Raessi and Pitsch)

Notations



Fluid model

- Incompressible Navier-Stokes equations in Ω_1 and Ω_2 :

$$\begin{aligned}\rho(\mathbf{u}_t + (\mathbf{u} \cdot \nabla)\mathbf{u}) &= -\nabla p + (\nabla \cdot \boldsymbol{\tau})^T + \rho \mathbf{g}, \\ \nabla \cdot \mathbf{u} &= 0\end{aligned}$$

- Continuity of velocity and velocity divergence:

$$\begin{aligned}[u] &= [v] = 0, \\ [(u_n, v_n) \cdot \mathbf{n}] &= 0.\end{aligned}$$

- Jump conditions on Γ :

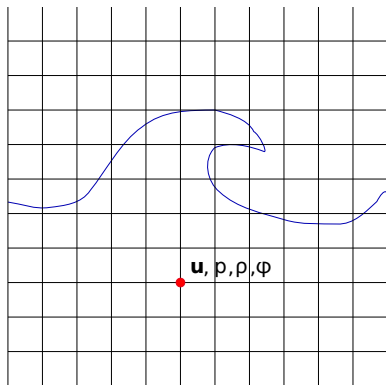
$$\begin{aligned}[\mu(u_n, v_n) \cdot \boldsymbol{\eta} + \mu(u_\eta, v_\eta) \cdot \mathbf{n}] &= 0, \\ [p] &= \sigma \kappa + 2[\mu](u_n, v_n) \cdot \mathbf{n}.\end{aligned}$$

- Material derivative of the velocity continuity

$$\left[\frac{\nabla p}{\rho}\right] = \left[\frac{(\nabla \cdot \boldsymbol{\tau})^T}{\rho}\right].$$

Discretization

- In the fluid, all variables on the same grid points
- Possible corrective term to avoid parasitic modes of the pressure



Numerical scheme in the fluid

Predictor-corrector scheme:

- Prediction (we take $p = 0$)

$$\frac{\mathbf{u}^* - \mathbf{u}^n}{\Delta t} = -[(\mathbf{u} \cdot \nabla)\mathbf{u}]^{n+\frac{1}{2}} + \frac{(\nabla \cdot \boldsymbol{\tau}^n)^T}{\rho} - \mathbf{g}$$

- Resolution of elliptic equation

$$\nabla \cdot \left(\frac{1}{\rho} \nabla p \right) = \frac{\nabla \cdot \mathbf{u}^*}{\Delta t}$$

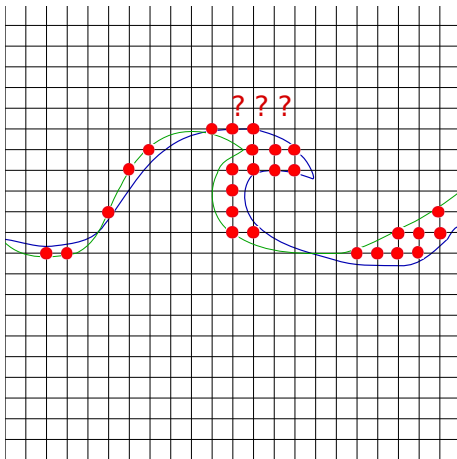
- Correction

$$\mathbf{u}^{n+1} = \mathbf{u}^* - \frac{\Delta t}{\rho} \nabla p$$

Why do we take $p = 0$ in prediction step?

$$[p] = \sigma\kappa + 2[\mu](u_n, v_n) \cdot \mathbf{n}.$$

$\Rightarrow p$ possibly discontinuous if the interface crosses a grid point during Δt



Numerical scheme in the fluid

- Prediction

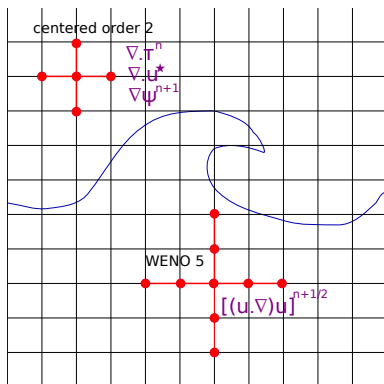
$$\frac{\mathbf{u}^* - \mathbf{u}^n}{\Delta t} = -[(\mathbf{u} \cdot \nabla)\mathbf{u}]^{n+\frac{1}{2}} + \frac{(\nabla \cdot \boldsymbol{\tau}^n)^T}{\rho} - \mathbf{g}$$

- Elliptic equation:

$$\nabla \cdot \left(\frac{1}{\rho} \nabla p \right) = \frac{\nabla \cdot \mathbf{u}^*}{\Delta t}$$

- Correction :

$$\mathbf{u}^{n+1} = \mathbf{u}^* - \frac{\Delta t}{\rho} \nabla p$$



Discretization near the interface

- Prediction

$$\frac{\mathbf{u}^* - \mathbf{u}^n}{\Delta t} = -[(\mathbf{u} \cdot \nabla)\mathbf{u}]^{n+\frac{1}{2}} + \frac{(\nabla \cdot \boldsymbol{\tau}^n)^T}{\rho} - \mathbf{g}$$

- Diffusion:

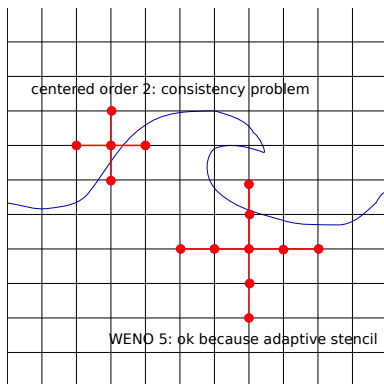
derivative of velocity discontinuous

⇒ lack of consistency

- Convection:

WENO 5 naturally adaptative,
continuous velocity

⇒ less worrying



Discretization near the interface

- Elliptic equation:

$$\nabla \cdot \left(\frac{1}{\rho} \nabla p \right) = \frac{\nabla \cdot \mathbf{u}^*}{\Delta t}$$

Discontinuity of ρ , jump conditions

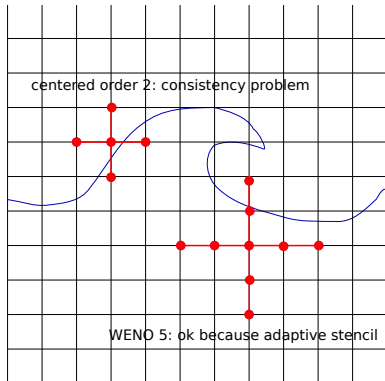
⇒ lack of consistency

- Correction :

$$\mathbf{u}^{n+1} = \mathbf{u}^* - \frac{\Delta t}{\rho} \nabla p$$

Discontinuity of ρ and ψ

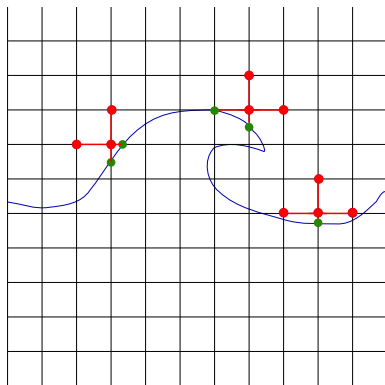
⇒ lack of consistency



Discretization near the interface

Our solution:

- Creation of **additional unknowns for u^* and p** on the interface, used for a sharp resolution of the pressure
- Regularization of μ and ρ **only** to account for viscous terms
→ no discontinuity any more in viscous terms



Discretization near the interface

- Elliptic problem

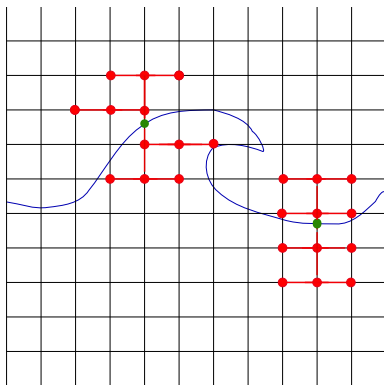
- In the fluid:

$$\nabla \cdot \left(\frac{1}{\rho} \nabla p \right) = \frac{\nabla \cdot \mathbf{u}^*}{\Delta t}.$$

(extrapolation of grid values for \mathbf{u}^*)

- On the interface:

$$\begin{aligned} [p] &= \sigma \kappa, \\ \left[\frac{\nabla p}{\rho} \right] &= 0. \end{aligned}$$



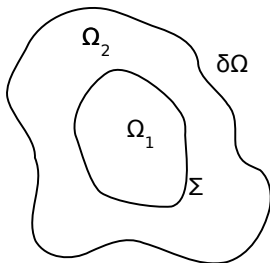
Interlude: elliptic problems with immersed interfaces

$$\nabla \cdot (k \nabla u) = f \text{ on } \Omega = \Omega_1 \cup \Omega_2$$

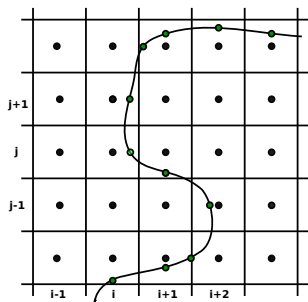
$$[[u]] = \alpha \text{ on } \Sigma$$

$$[[k \frac{\partial u}{\partial n}]] = \beta \text{ on } \Sigma$$

$$u = g \text{ on } \delta\Omega$$



Discretization strategy



Creation of additional unknowns on the interface:

- used to discretize the elliptic operator on each side of the interface
- obtained by a discretization of jump conditions across the interface

Which accuracy is needed near the interface?

To obtain a second order convergence (in max norm), we need:

- a first-order truncation error for the elliptic operator near the interface
⇒ avoid linear extrapolations (for instance: ghost-cell like)
- a second-order truncation error of the fluxes discretization
⇒ use of an expanded stencil

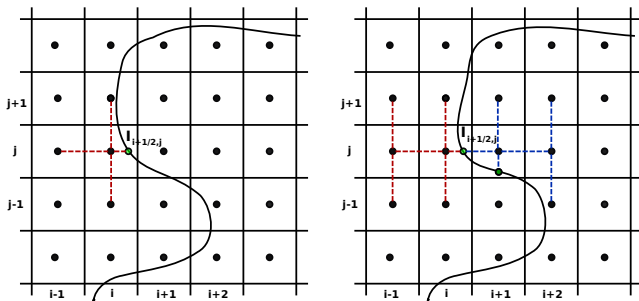


Figure: Examples of stencils for the discretization of elliptic operator and fluxes on each side of the interface.

Rising of a small air bubble in water

Water: $\rho = 1000 \text{ kg/m}^3$, $\mu = 1,137 \cdot 10^{-3} \text{ kg/ms}$,

Air: $\rho = 1 \text{ kg/m}^3$, $\mu = 1,78 \cdot 10^{-5} \text{ kg/ms}$,

$\sigma = 0.0728 \text{ kg/s}^2$, bubble radius $1/300 \text{ m}$, $Tf = 0.05 \text{ s}$.

Rising of a large air bubble in water

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$\sigma = 0.0728 \text{ kg/s}^2$, bubble radius $1/3 \text{ m}$, $Tf = 0.5 \text{ s}$.

Dam break problem

Water: $\rho = 1000 \text{ kg/m}^3$, $\mu = 1,137 \cdot 10^{-3} \text{ kg/ms}$,

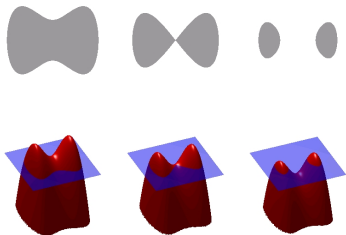
Air: $\rho = 1,226 \text{ kg/m}^3$, $\mu = 1,78 \cdot 10^{-5} \text{ kg/ms}$,

$\sigma = 0.0728 \text{ kg/s}^2$, height of water column $h = 5.715 \text{ cm}$, domain $40 \times 10 \text{ cm}$

Sharp capture of the interface: level-set approach

- Γ captured as $\{\phi = 0\}$ with ϕ defined over Ω ,
- easily handle complex geometries,
- straightforward computation of geometric properties:

$$\mathbf{n} = \nabla\phi, \quad \kappa = \nabla \cdot \left(\frac{\nabla\phi}{|\nabla\phi|} \right),$$



- transport of Γ with the flow \mathbf{u} ,
- in practice, ϕ is the signed distance to Γ ($\Rightarrow |\nabla\phi| = 1, \kappa = \Delta\phi$).

Reminder: elliptic problem with jumps on the interface

- Elliptic problem

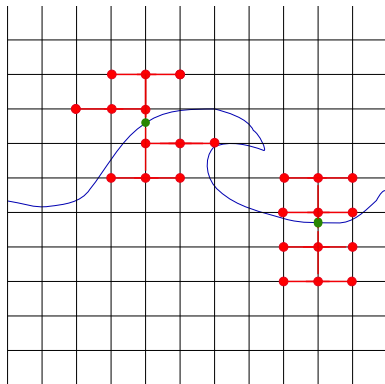
- In the fluid:

$$\nabla \cdot \left(\frac{1}{\rho} \nabla p \right) = \frac{\nabla \cdot \mathbf{u}^*}{\Delta t}.$$

(extrapolation of grid values for \mathbf{u}^*)

- On the interface:

$$\begin{aligned} [p] &= \sigma \kappa, \\ \left[\frac{\nabla p}{\rho} \right] &= 0. \end{aligned}$$

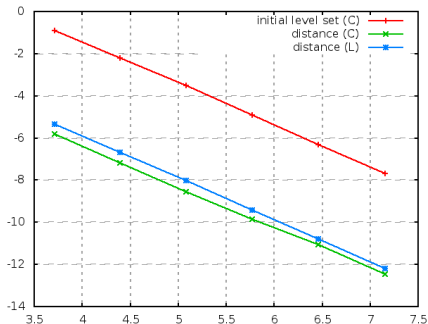


↪ consistent (at least first-order) scheme for κ required.

Why using the distance function?

Objective: ensure consistency for the computation of κ AND low amplitude of the error.

- Example of computation of the curvature of a circle (second order FD formulas):
- with a level-set function with large and small gradients, $\nabla \cdot \left(\frac{\nabla \phi}{|\nabla \phi|} \right)$,
- with the distance function, $\nabla \cdot \left(\frac{\nabla \phi}{|\nabla \phi|} \right)$,
- with the distance function, $\Delta \phi$,
- **reduction of the error by a factor 100.**



Standard approach

- transport of ϕ with \mathbf{u} , e.g.

$$\phi^* = \phi^n - \Delta t \mathbf{u}^n \nabla \phi^n,$$

- every 5 or 10 steps, reinitialize ϕ^* , e.g. with

$$\partial_\tau \phi + \text{sign}(\phi^*) (|\nabla \phi| - 1) = 0,$$

$$\phi|_{\tau=0} = \phi^*.$$

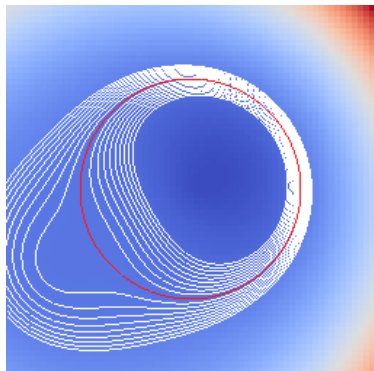
- RK3-TVD scheme for τ , t , WENO-5 scheme for $\nabla \phi$,

- $\Delta \tau = \frac{\Delta x}{2}$.

Main issues:

- WENO-5 scheme for reinitialization is not accurate enough near the interface,
- too many reinitialization steps,
- reinitialization steps might be too expensive.

Test case with large and small gradients



$$d = \sqrt{x^2 + y^2} - r_0$$

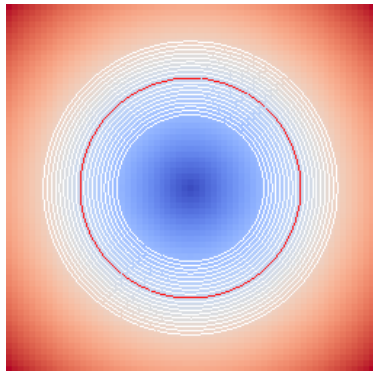
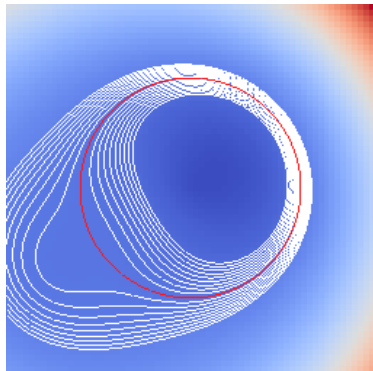
$$\phi_0 = \frac{d}{r_0} (\epsilon + (x - x_0)^2 + (y - y_0)^2)$$

$$\Omega = (-1, 1)^2$$

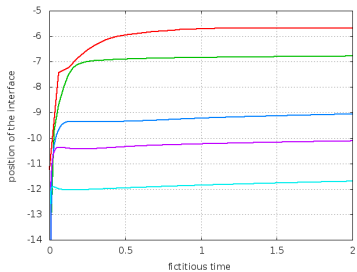
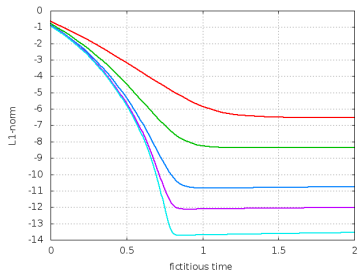
$$r_0 = 0.6$$

$$\epsilon = 0.1, x_0 = -0.7, y_0 = -0.4$$

Test case with large and small gradients



Accuracy of the standard approach



Reducing interface displacement

Main issue : WENO scheme uses informations on the wrong side of the interface

Subcell fix (Russo & Smereka)

Modify scheme near the interface :

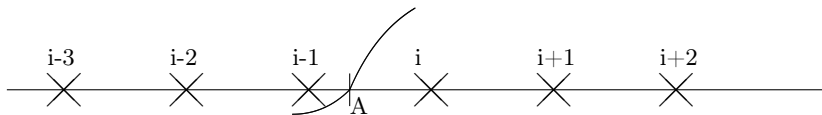
$$\phi_{i,j}^{n+1} = \phi_{i,j}^n - \frac{\Delta\tau}{\Delta x} (\text{sign}(\phi_{i,j}^0) |\phi_{i,j}^n| - d_{i,j}^n),$$

$d_{i,j}^n$ approximate value of the signed distance.

\rightsquigarrow 2nd order for the position of the interface.

Main idea : use informations on the interface (almost upwind scheme)

Reducing interface displacement (high order)



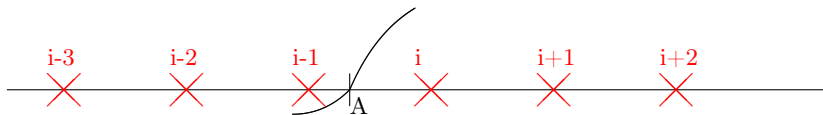
Standard WENO-5 stencil for $D_x^- \phi_i : (x_{i-3}, x_{i-2}, \dots, x_{i+2})$

Use point A in the stencil : $(x_{i-2}, x_{i-1}, x_A, x_i, x_{i+1}, x_{i+2})$.

ENO scheme of high-order (Russo & Smereka, Gibou *et al*, Sussman & Fatemi).

- Away from the interface, use WENO scheme,
- close to the interface, use subcell fix with ENO scheme.

Reducing interface displacement (high order)



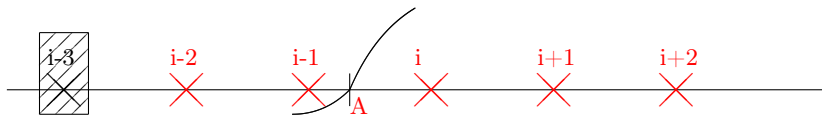
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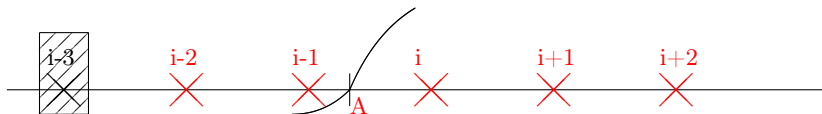
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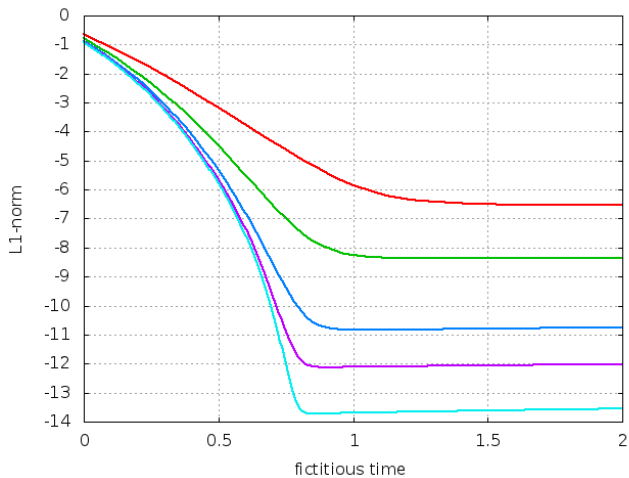
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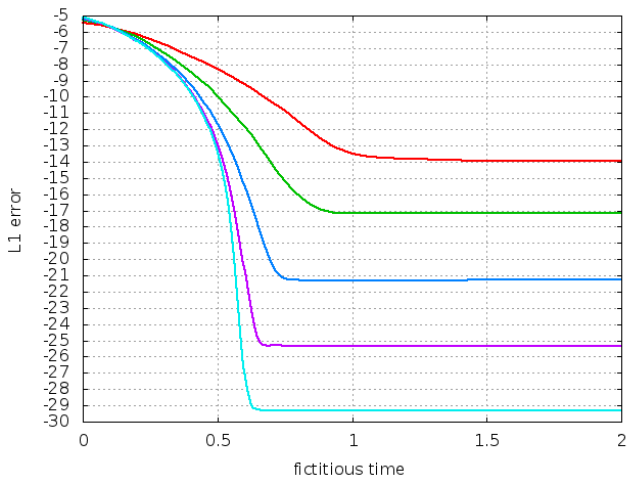
- Away from the interface, use WENO scheme,
- close to the interface, use subcell fix with ENO scheme.

Global accuracy



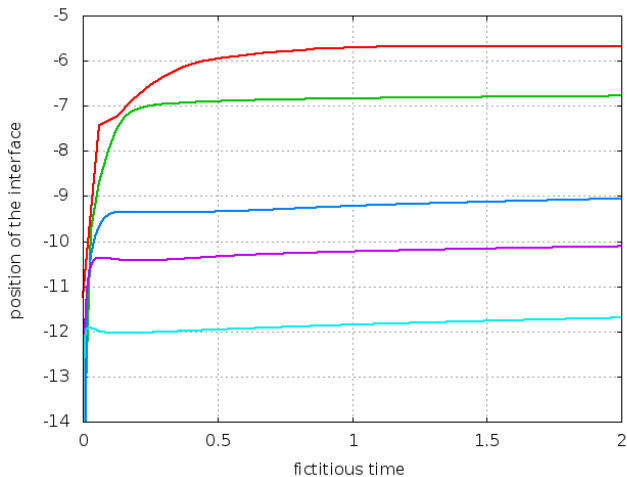
WENO scheme

Global accuracy



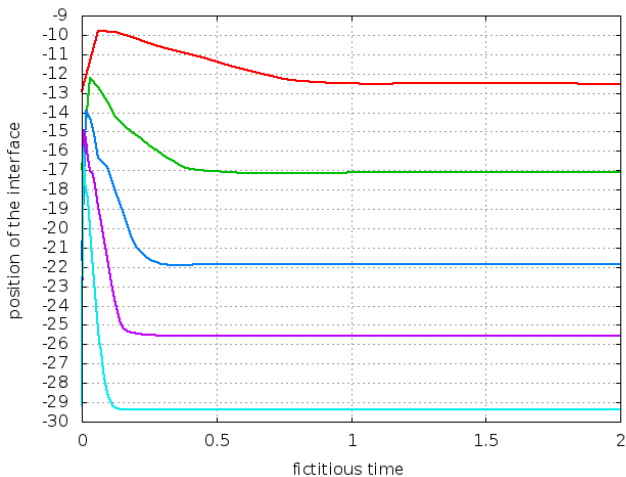
Subcell fix of order 3

Accuracy near the interface



WENO scheme

Accuracy near the interface



Subcell fix of order 3

Coupling with transport

$$\Omega = (0, 1)^2$$

$$\phi|_{t=0} = \sqrt{((x - 0.5)^2 + (y - 0.75)^2)} - 0.15$$

$$\mathbf{u} = \cos\left(\frac{\pi t}{T}\right) \nabla^\perp \omega$$

$$\omega = \sin(\pi x)^2 \sin(\pi y)^2$$

Coupling with transport (naive approach)

- evaluate spatial error in the scheme,
- previous example with $T = 0.046875$, results for $t = T$,
- $\Delta t = \Delta x^2$.

Δx	every time step		only 5 reinitializations	
	err.	coc	err.	coc
1/16	1.59e-02	-	2.76e-02	-
1/32	5.07e-03	1.65	5.05e-03	2.45
1/64	1.46e-04	5.12	8.48e-05	5.90
1/128	3.22e-05	2.18	2.50e-06	5.09
1/256	1.64e-04	-2.35	1.83e-07	3.77

Table: L^∞ error near the computed interface

⇒ avoid reinitialization at every time step

How to control the number of reinitializations?

- Introduce $r_g := |||\nabla\phi| - 1|||$,
- $r_g = 0$ for ϕ a distance function,
- while $r_g < \varepsilon$, use only transport for ϕ ,
- once $r_g \geq \varepsilon$, replace ϕ by the distance function.

mesh	L^∞ error	coc	L^∞ error	coc
40	0.919E+00	-	0.108E+01	-
80	0.291E+00	1.66	0.363E+00	1.57
160	0.934E-01	1.64	0.921E-01	1.98
320	0.301E-01	1.64	0.343E-01	1.43
640	0.369E-02	3.03	0.422E-02	3.02

Table: Previous example with $T=2$, $\varepsilon = 0.1$. L^∞ -errors on the curvature of the interface: at $t = 2$ (left) and $t = 4$ (right). For each computation : 16 reinitializations.

Numerical illustration

Figure: Previous example with $T = 6$ (600 time steps), $\varepsilon = 0.15$: without reinitialization (left), naive approach (middle, 600 reinitializations) and new strategy (right, 14 reinitializations).

Final strategy

Strategy based on the approximation of a continuous problem:

- *initialization*: start with ϕ the signed distance function,
- *transport*: as long as $r_g < \varepsilon$, evolve ϕ according to

$$\partial_t \phi + \mathbf{u} \cdot \nabla \phi = 0,$$

- *reinitialization*: if $r_g = \varepsilon$, replace ϕ by the distance function; go to transport.

Pros

- third order convergence for ϕ , first order convergence for κ ,
- ϕ remains close to a distance function \Rightarrow lower amplitudes of the error on κ .

Cons

- choice of ε ,
- requires a full computation of the distance function. Relaxation might be expensive \Rightarrow coupling relaxation method and fast-sweeping scheme away from the interface.

Add-on: Fast-Sweeping step

Analogy with linear systems

Relaxation method \leftrightarrow relaxed Jacobi method,
(very accurate near the interface, but slow),

Fast-Sweeping method \leftrightarrow Gauss-Seidel method,
(very fast, but requires a good guess near the interface).

In practice

- Use relaxation method in a band of length $5\Delta x$,
- iterate until convergence in the narrow band,
- then Fast-Sweeping away from the interface,
- second order FS, with fixed number of iterations.

Add-on: numerical illustration

Previous reinitialization example.

mesh	$\ d - \phi_h\ $	coc	$\ \kappa - \kappa_h\ $	coc	number of it.
40	6.14E-04	-	5.97E-02	-	23
80	5.28E-05	3.54	2.65E-02	1.17	28
160	5.60E-06	3.24	1.25E-02	1.08	32
320	6.47E-07	3.11	6.29E-03	1.00	36
640	8.44E-08	2.94	3.17E-03	0.99	41

Table: Errors and computed order of convergence (coc) for the mixed method. L^∞ -error in the narrow band on ϕ (left), L^∞ -error on κ on the interface (middle) and total number of iterations (right).

- (not shown here) second order accuracy for the global error on ϕ ,
- with only relaxation, number of iterations $\sim 2/\Delta x$.

Conclusion

- Development of sharp cartesian method for air-water interfaces with a second order treatment of the pressure,
- High order level-set technique, allowing consistent computation of the curvature of the interface, even for long times.

What's next:

- Coupling of the two techniques,
- Implementation, validation in 3D,
- Application to fluid-solid interaction.