



A Versatile Sharp Interface Immersed Boundary Method with Application to Complex Biological Flows

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Mechanical Engineering

JOHNS HOPKINS
U N I V E R S I T Y

Biological Flows

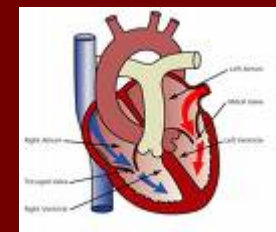
■ Biomimetics and Bioinspired Engineering

- What can we learn from Nature ?
- How can we adapt Nature's solutions into engineered devices/machines ?



■ Biomedical Engineering

- Cardiovascular flows
- Respiratory flows
- Phonatory/Speech Mechanisms
- Biomedical Devices



Inspiration from Dragonflies

■ Dragonflies

- Existed for 350 million years
- Wingspan from 2 – 80 cm
- Fast and agile

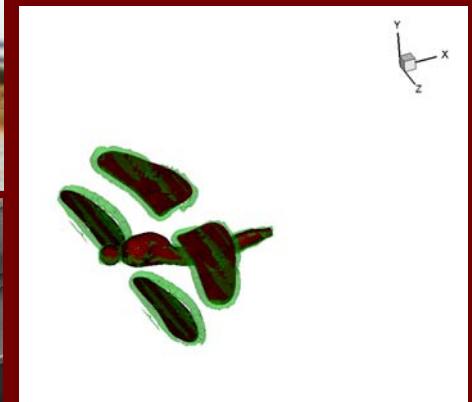
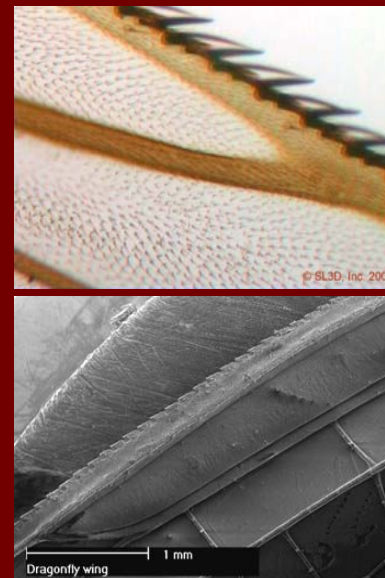
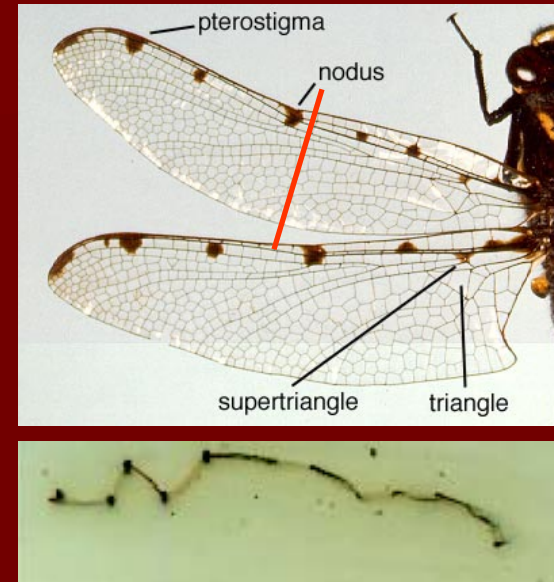
■ Wing Design

- Thin, lightweight
- Vein reinforced
- Pleated along chord
- Pterostigma
- Microstructure

■ Wing Configuration

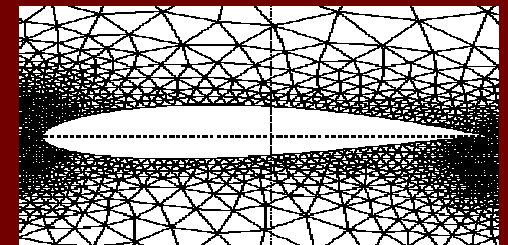
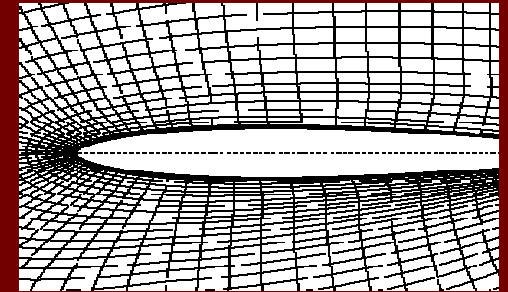
- Wing-wing interaction?

■ Wing Flexion?



Computational Modeling

- Need to tackle
 - Complex 3D geometries
 - Moving boundaries
 - Fluid Structure Interaction
 - Resolution of vortex dynamics
 - Relatively low Reynolds numbers
- Very challenging for conventional body fitted methods.
- Immersed Boundary Methods
 - handle these problems in all their complexity.



ViCar3D

Journal of Computational Physics
Volume 227, Issue 10, 1 May 2008,
Pages 4825-4852

Viscous Cartesian Grid Solver for 3D Immersed Boundaries

■ Simulations on non-conforming Cartesian Grids

- Stationary/moving boundaries
- Solids/membranes

■ Sharp Interface IBM method

- No boundary forcing (Peskin et al)
- 3D ghost-cell methodology

■ 2nd Order Fractional Step Scheme

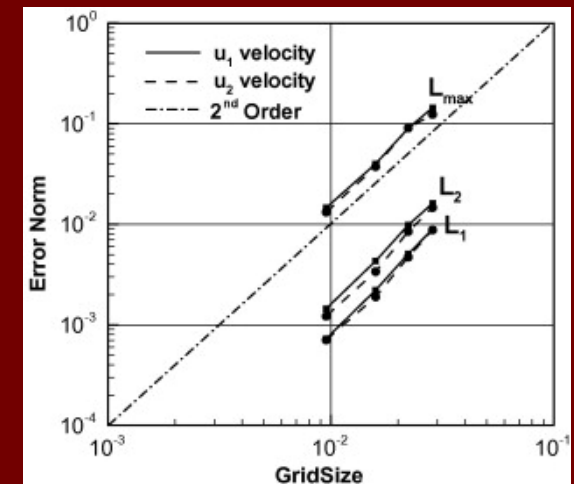
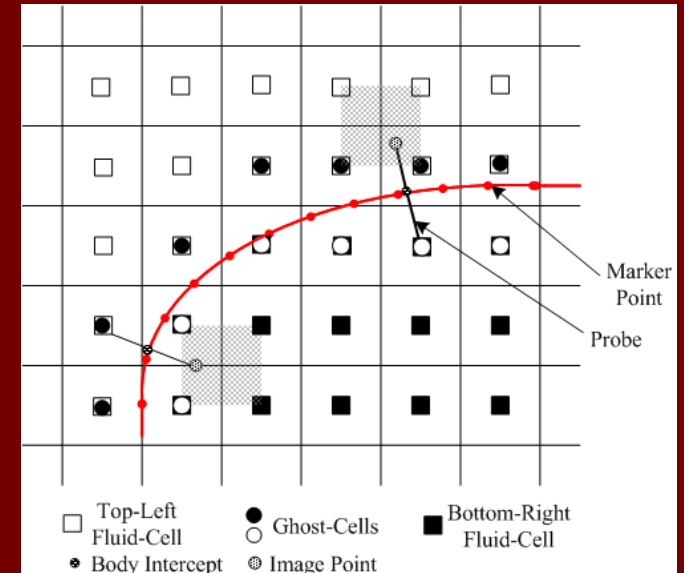
■ 2nd Order non-dissipative central difference scheme

- IBM treatment also 2nd order accurate

■ Non-uniform meshes

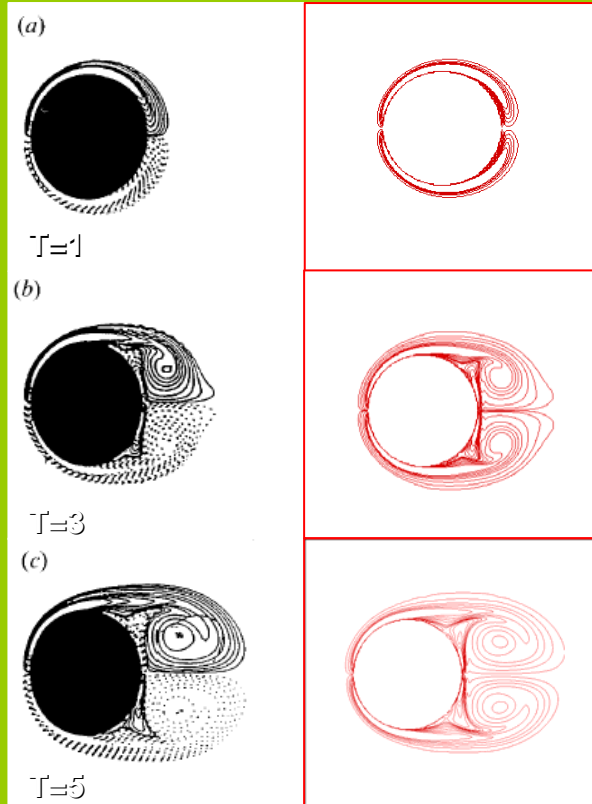
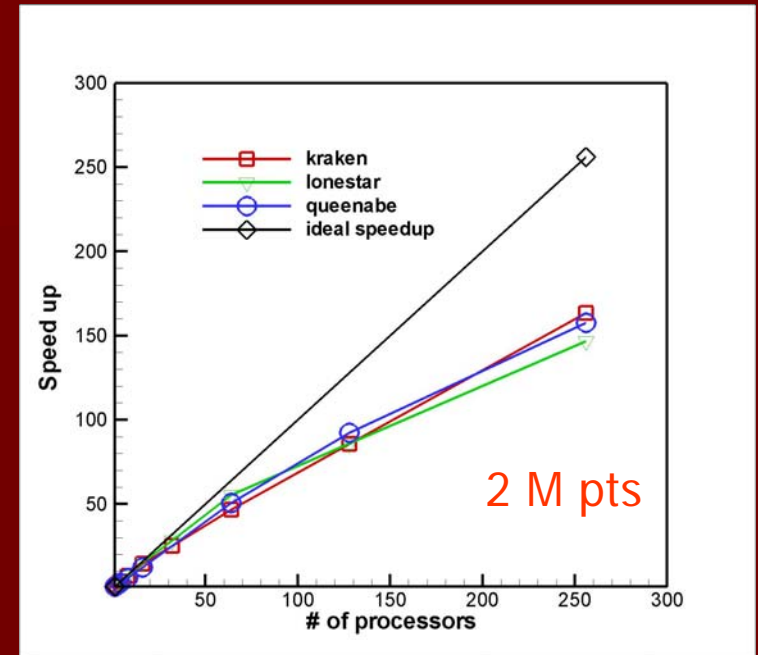
■ Geometric Multigrid for Pressure Poisson

■ Global Coeff Dynamic SGS Model (Vreman)



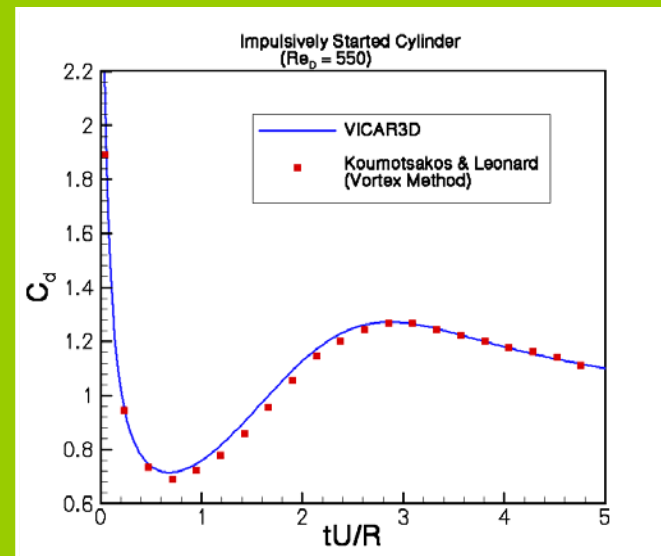
ViCar3D

- Parallelized
- Extensively validated



Komoutsakos & Leonard

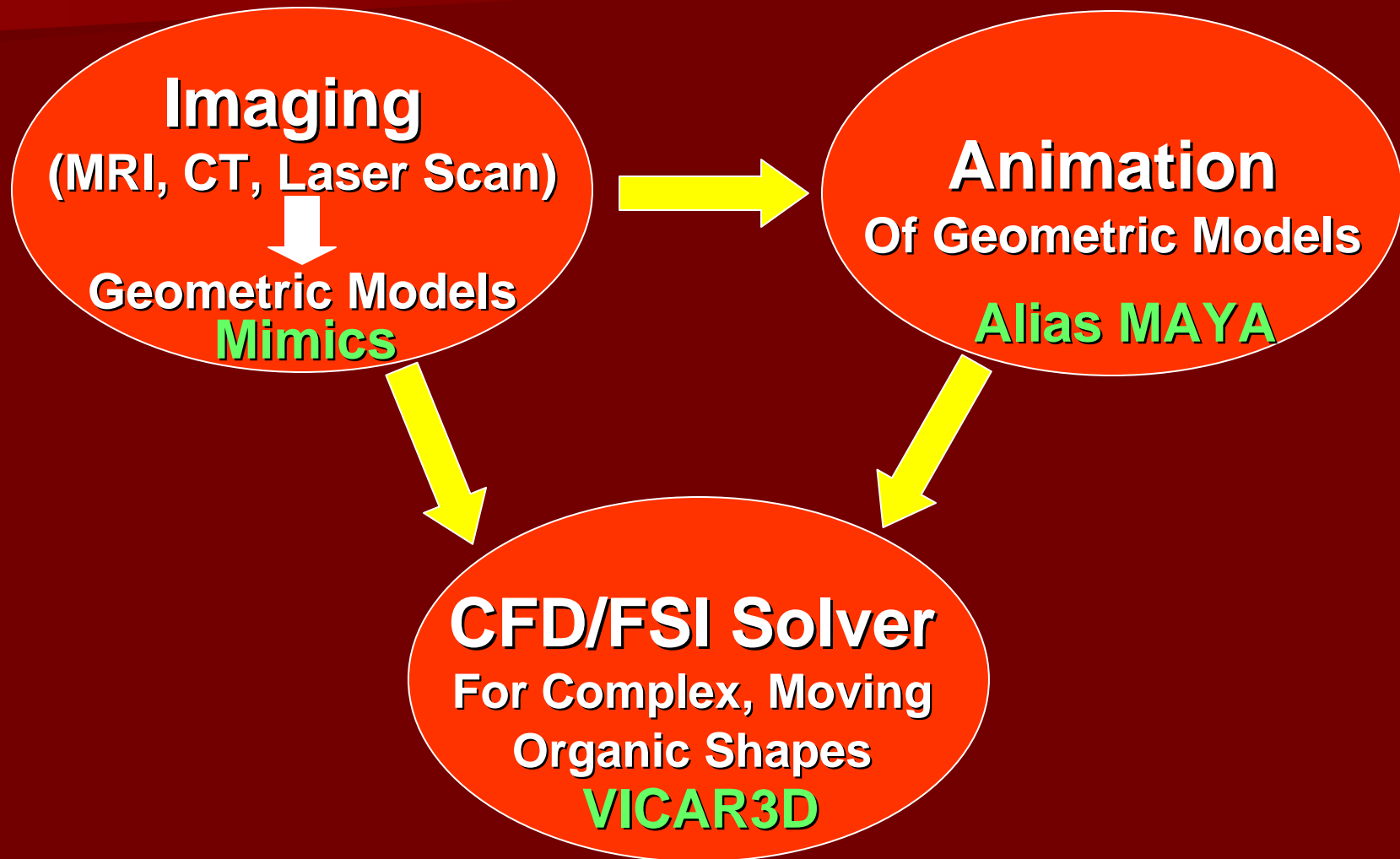
VICAR3D



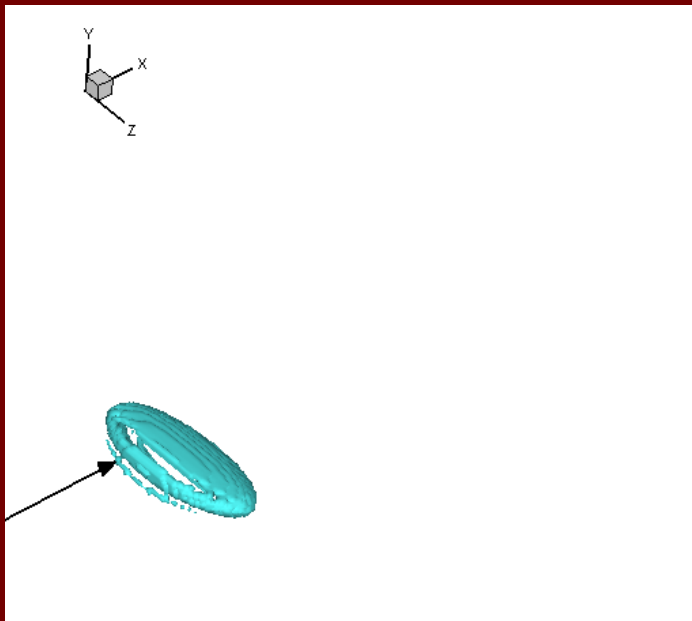
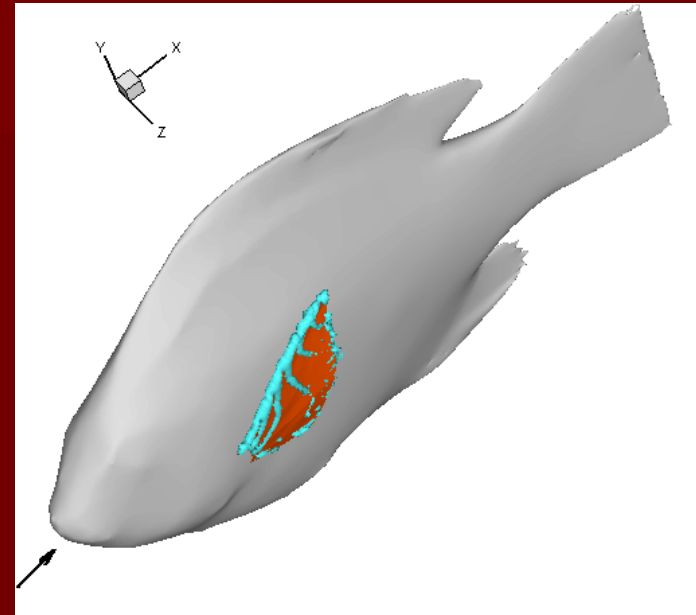
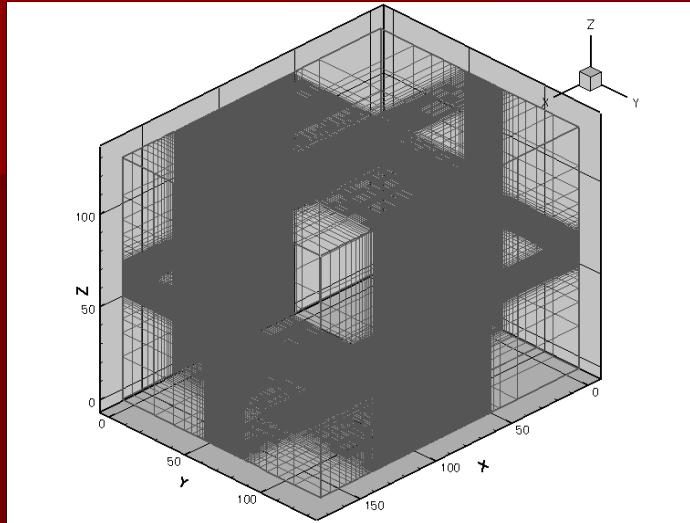
Impulsively Started Cylinder
 $Re=1000$

Mittal et al
 2008, JCP

Closing the Loop for CFD in Biology/Biomedical Engineering

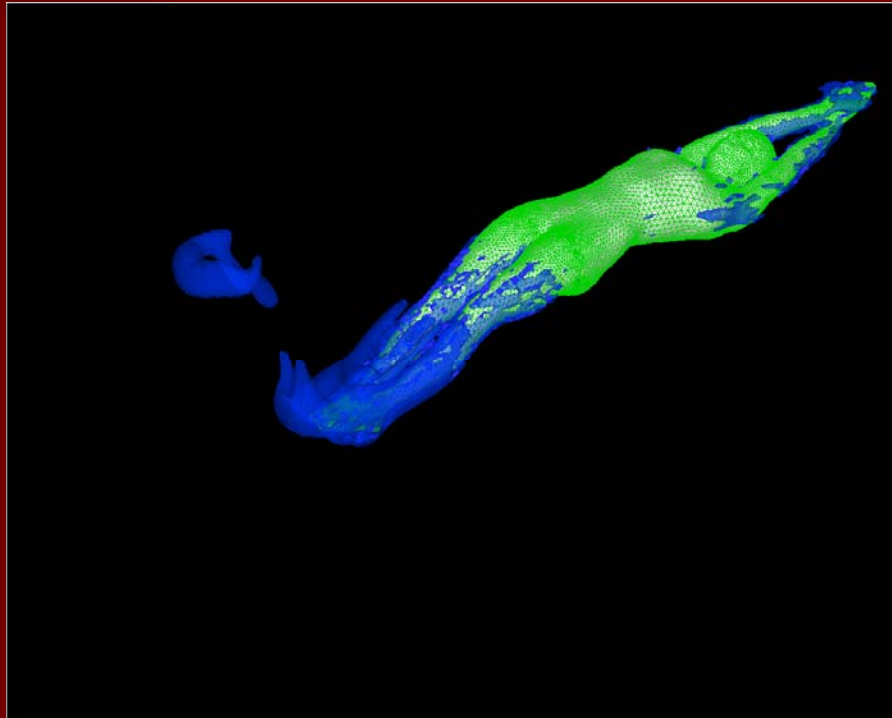


ViCar3D-Capabilities

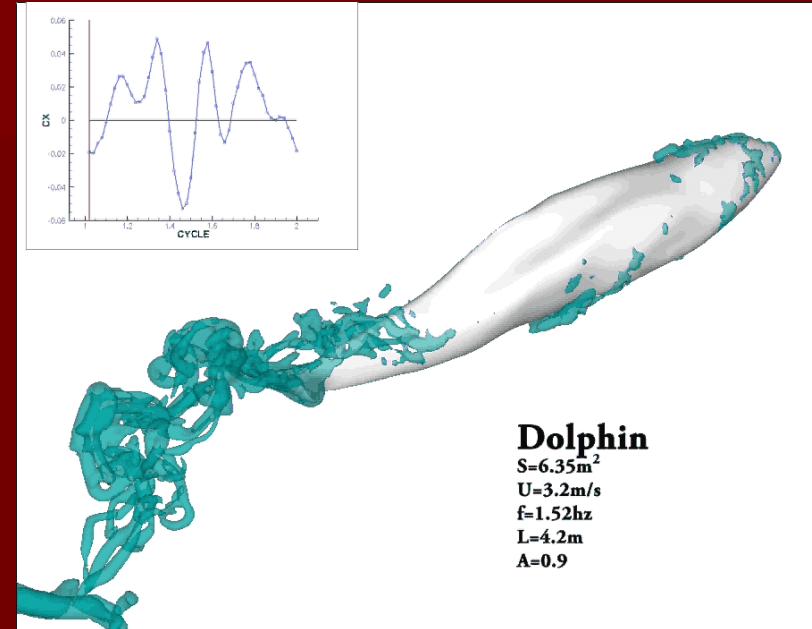


- "Wake Topology and Hydrodynamic Performance of Low-Aspect-Ratio Flapping airfoil", J. Fluid Mechanics (2006) Vol 566 pp 309-343 .
- Low-dimensional models and performance scaling of a highly deformable fish pectoral fin; J. Fluid Mech. (2009), vol. 631, pp. 311–342.
- "Computational modelling and analysis of the hydrodynamics of a highly deformable fish pectoral fin." (2010) , Journal of Fluid Mechanics , doi:10.1017/S0022112009992941.

ViCar3D-Capabilities



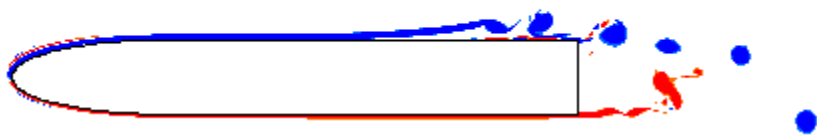
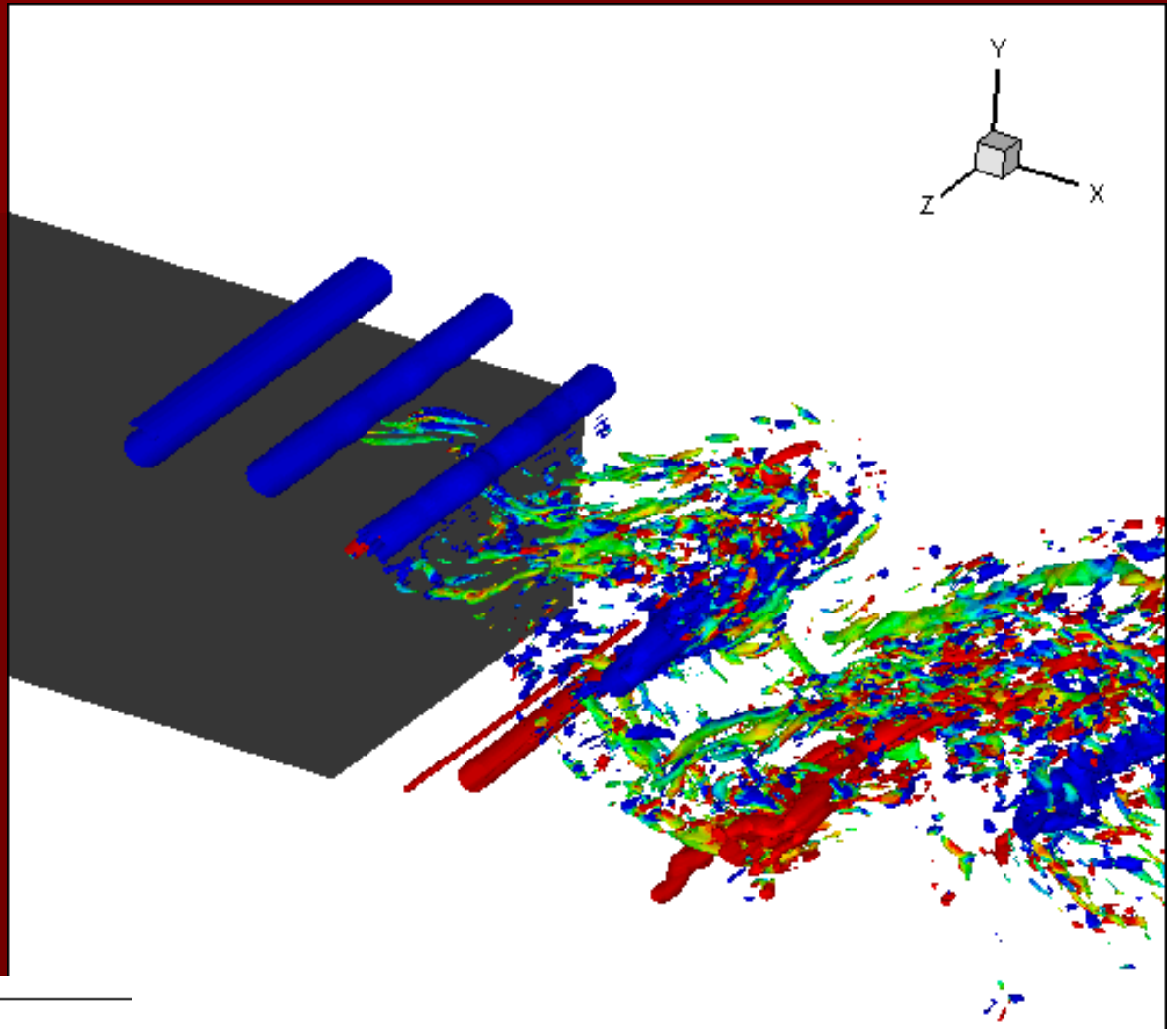
CFD of the dolphin kick



- "Propulsive Efficiency of the Underwater Dolphin Kick in Humans", Journal of Biomechanical Engineering, Vol. 131, May 2009
- "A computational method for analysis of underwater dolphin kick hydrodynamics in human swimming", Sports Biomechanics, 8(1), pp. 60-77, March 2009.
- "A comparison of the kinematics of the dolphin kick in humans and cetaceans", Human Movement Science, Vol.28, pp.99-112, 2009

High Re??

- $Re_c = 10^5$
- 512x256x32
- 128 CPUs



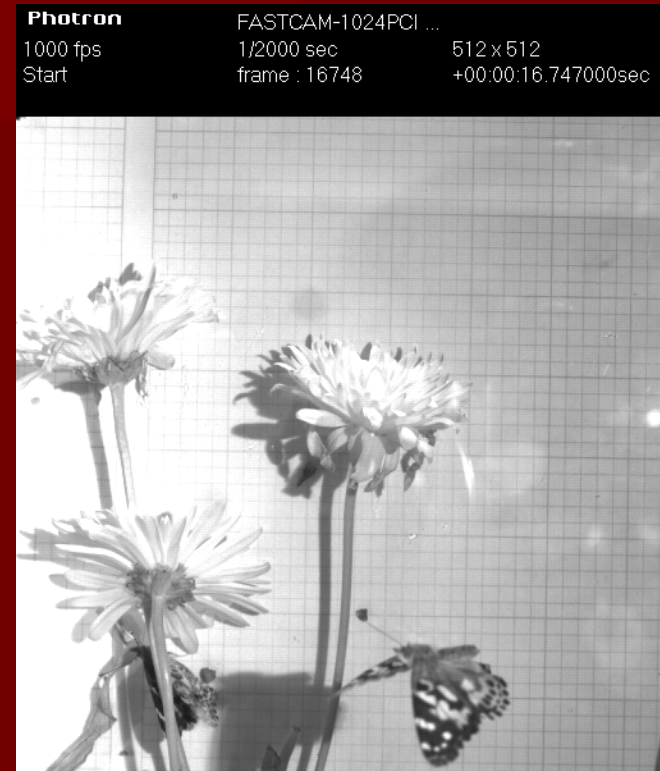
• Nonlinear dynamics and synthetic-jet-based control of a canonical separated flow. *J. Fluid Mech.*, doi:10.1017/S002211201000042X

Flight Maneuvers in Insects



Gravity

Side View



Top View

- Maneuver: change in heading and/or speed
- Insects display a large array of maneuvers

Flapping Frequency and Maneuvering

■ High frequency flappers ($f > 150$ Hz)

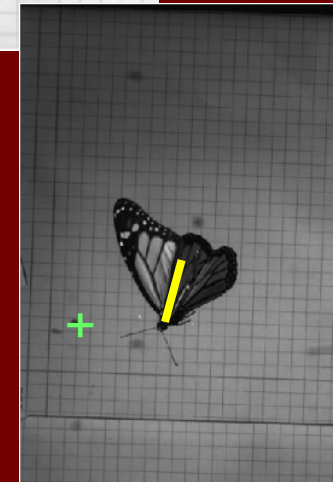
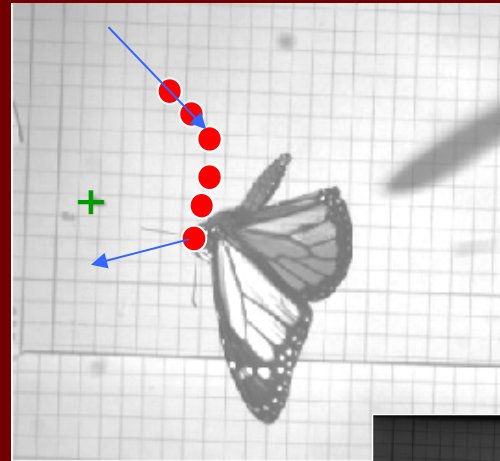
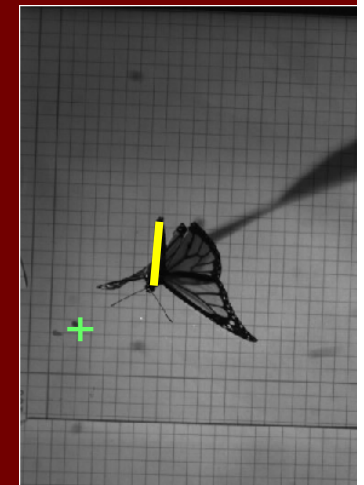
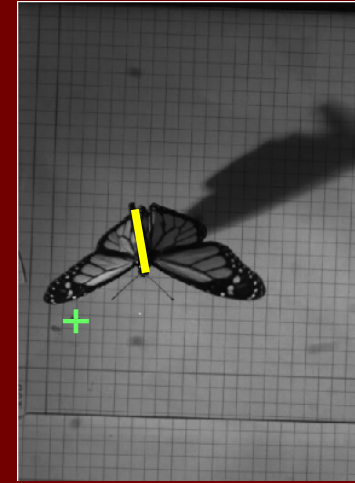
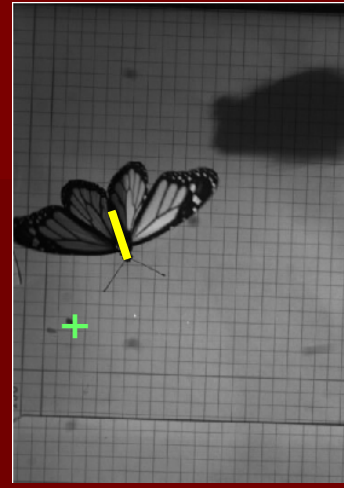
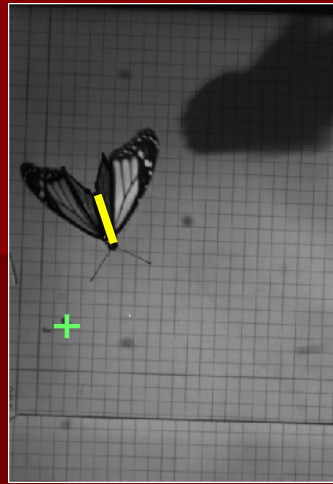
- Bees, Flies, wasps etc
- $\tau_{turn} > 10\tau_{flap}$
- Minute changes in kinematics required to execute turn. (Dickinson et al)
- Stroke plane/amplitude/pitch angle

$$T = I_{\theta\theta}\ddot{\theta} + C\dot{\theta}$$

$$\tau_{turn} \sim I_{\theta\theta} / C$$

■ Low frequency flappers ($f < 50$ Hz)

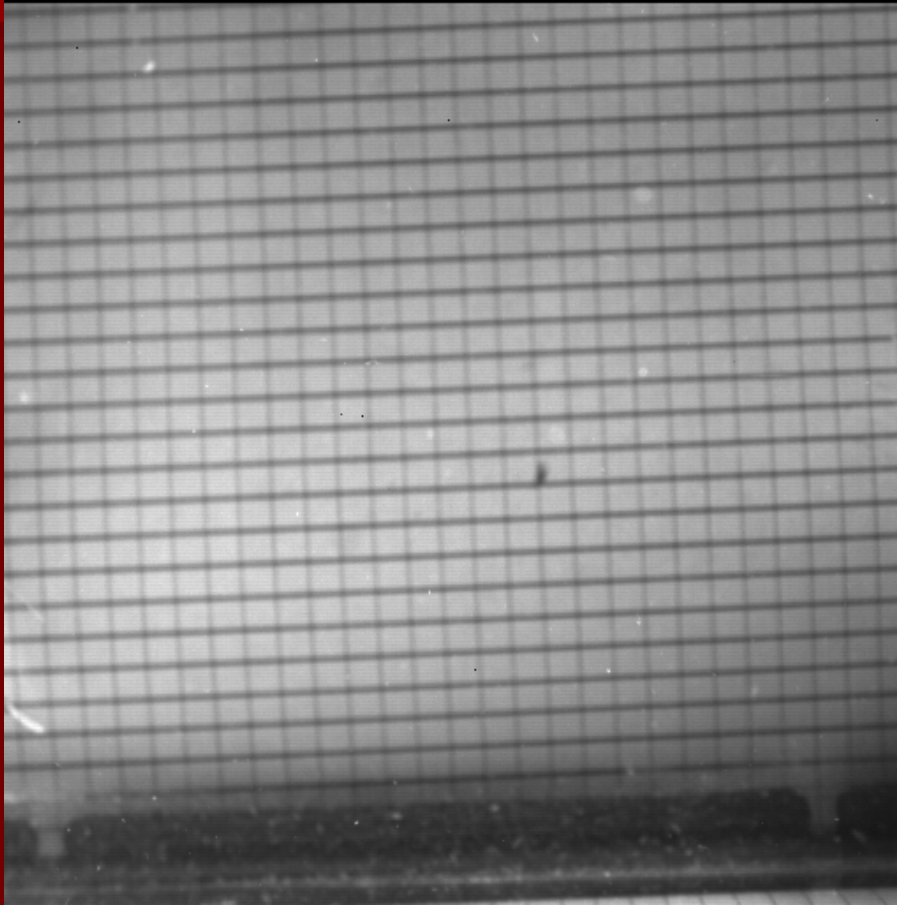
- Moths, butterflies, locusts etc.
- $\tau_{turn} \sim \tau_{flap}$
- Turns can be executed in $O(1)$ flap if wings can produce sufficient turning moments.
- Does this happen??



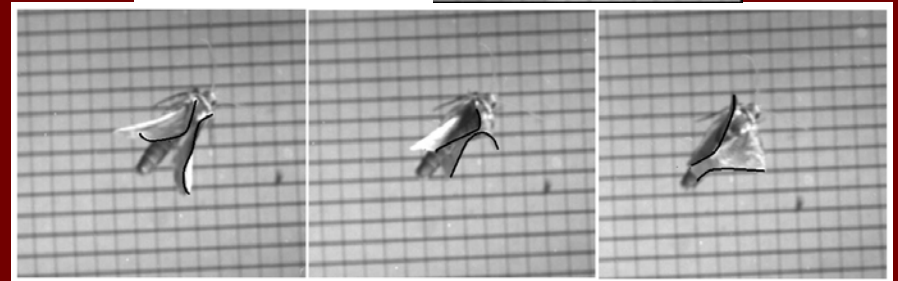
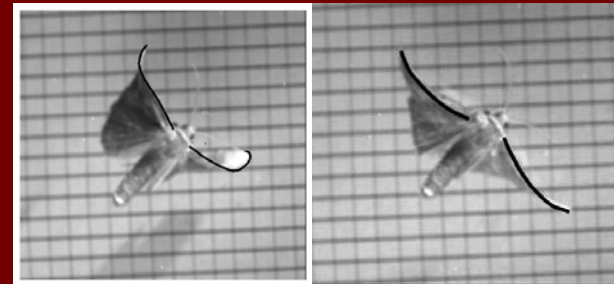
- Turning in a Monarch Butterfly
- Sequence shows 1.5 flaps
- $>90^\circ$ change in heading !
- Turning distance $<$ body size
- Turn on a dime!

Wing Flexion: Enabler of other Flight Modes

Photron FASTCAM-1024PCI ...
1000 fps 1/4000 sec 512 x 512
Start frame : 800 +00:00:00.799000sec



Moth in Climbing Flight



Clap & peel enabled by
wing flexion

COBRE Insect Videogrammetry Lab

Integrated Approach

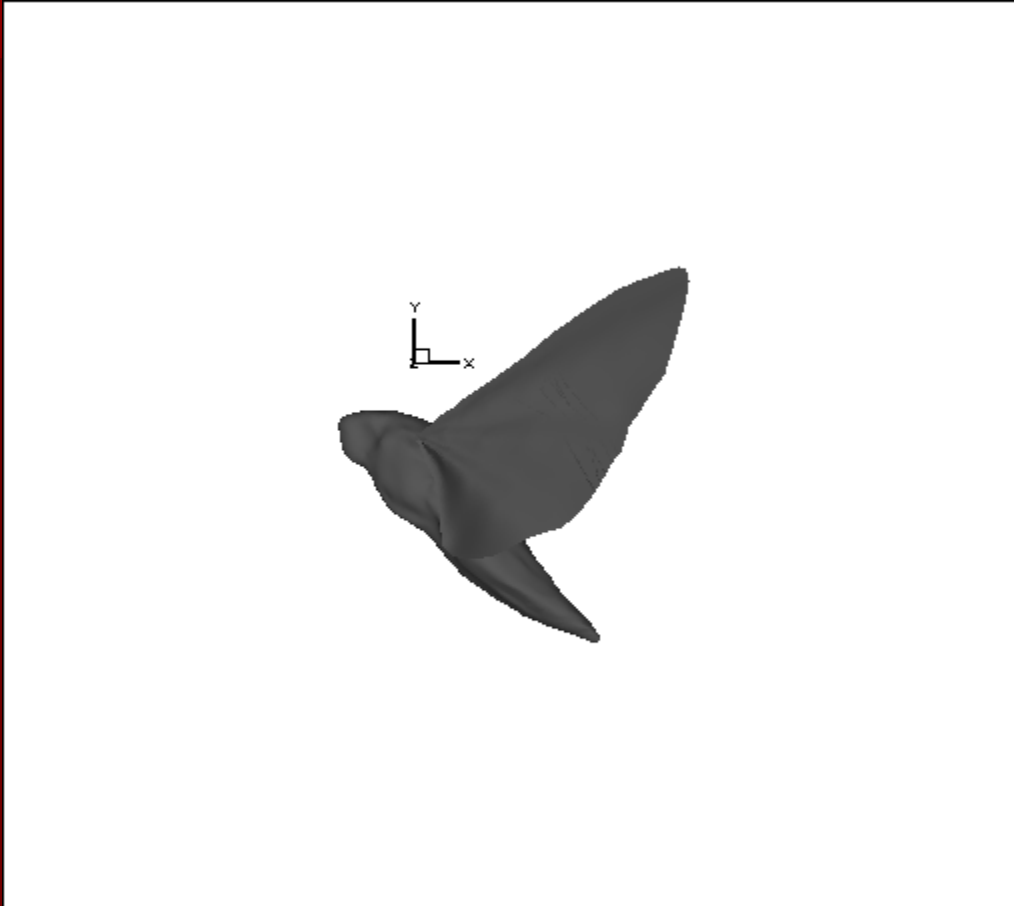
- High Speed Videogrammetry
 - JHU Laboratory for Bioinspired Engineering
 - Tyson Hedrick Lab (UNC)
- Structural parameterization (Vallance Lab, GWU)
 - Wing
 - Body
- High Fidelity Computational Modeling of Aerodynamics and Aero-Structural Interaction
 - Sharp Interface Immersed Boundary Method
 - Direct and Large-Eddy Simulation
 - Wing deformation modeling using FEM

Hawkmoth in Hover



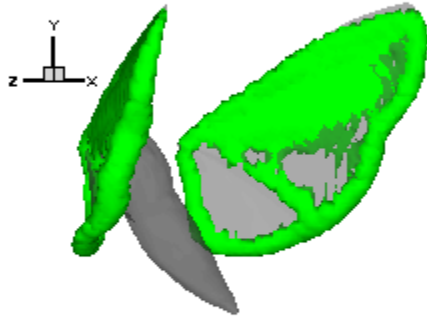
Hedrick Lab (UNC)

Animated Model Rendered for CFD



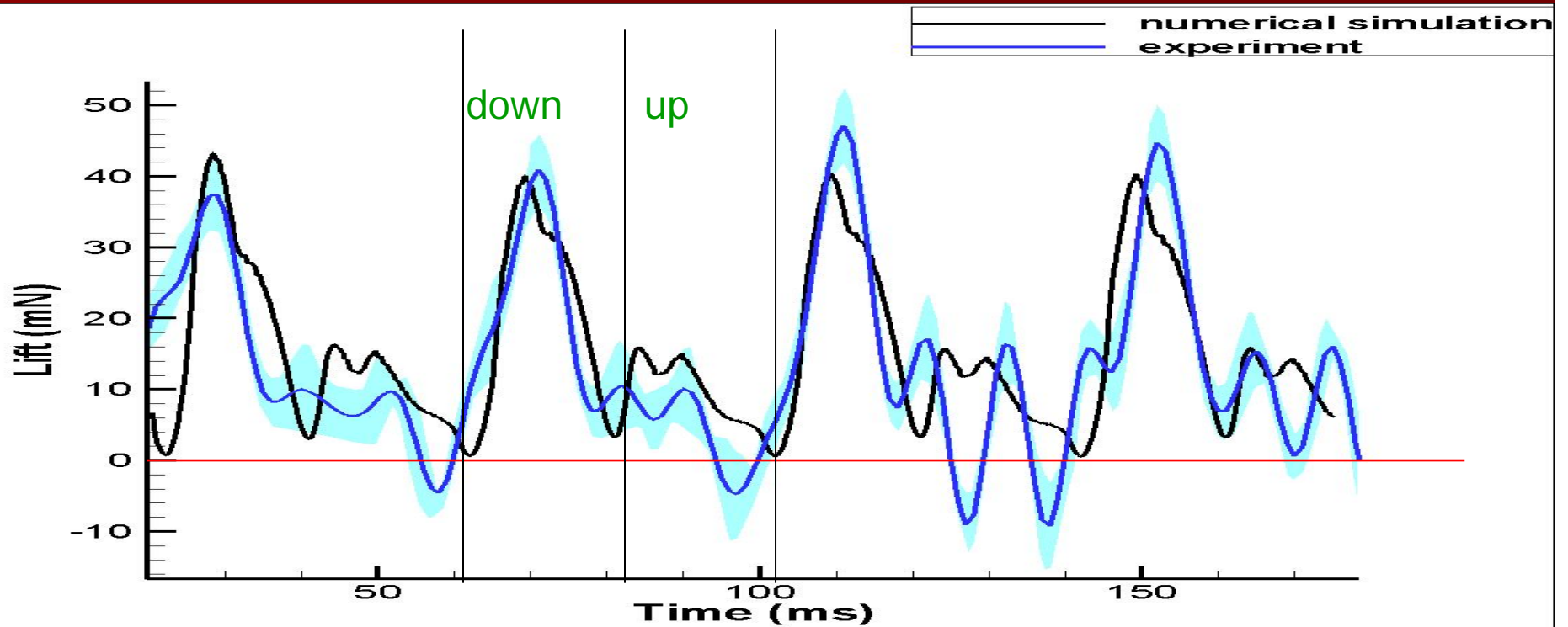
- Moth body based on high-res laser scan.
- Animation created in MAYA by matching high speed video.

Vortex Dynamics



- Strong spiral LEV on downstroke.
- Vortex ring shed at the end of downstroke from each wing.
- Weak LEV on upstroke

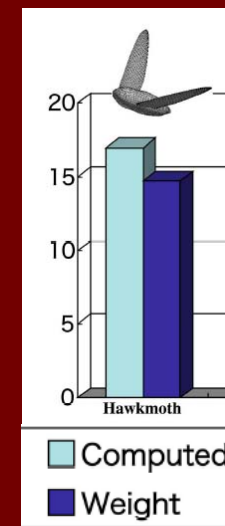
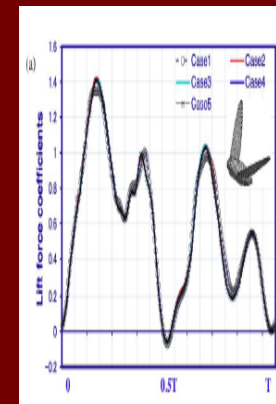
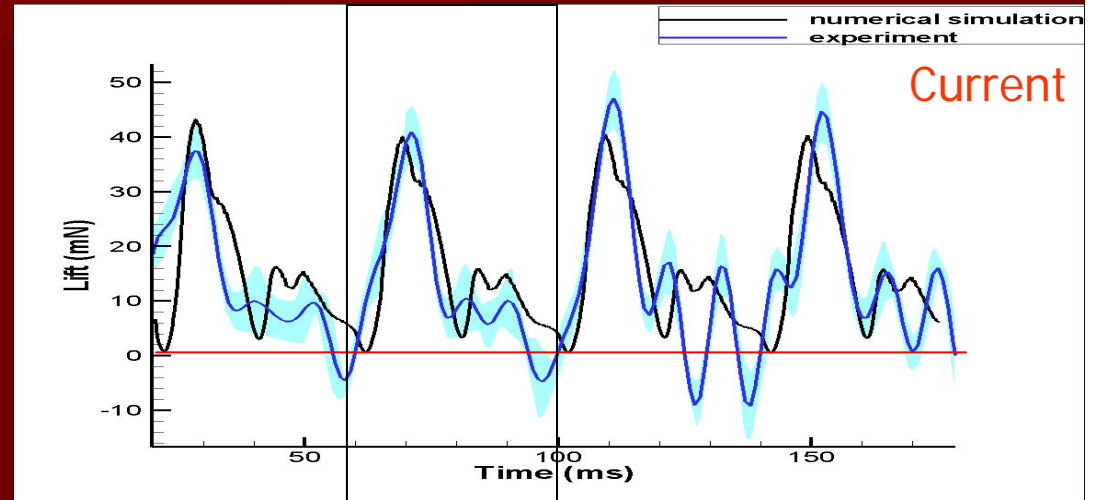
Lift Prediction



- Fairly good prediction of peak thrust during downstroke.
- Some mismatch during upstroke
 - Larger cycle-to-cycle variations in upstroke
- Interestingly, upstroke is found to be quite ineffective!

Comparison with Past Models

- Liu et al (Chiba University)
- Hawkmoth in hover
- Rigid wings
- Kinematics based on Ellington's data.
- Average lift is comparable
- However simulations show significant lift generation during up (back) stroke.
- Possibilities?
 - Discrepancy in kinematics
 - Rigid versus deformable?

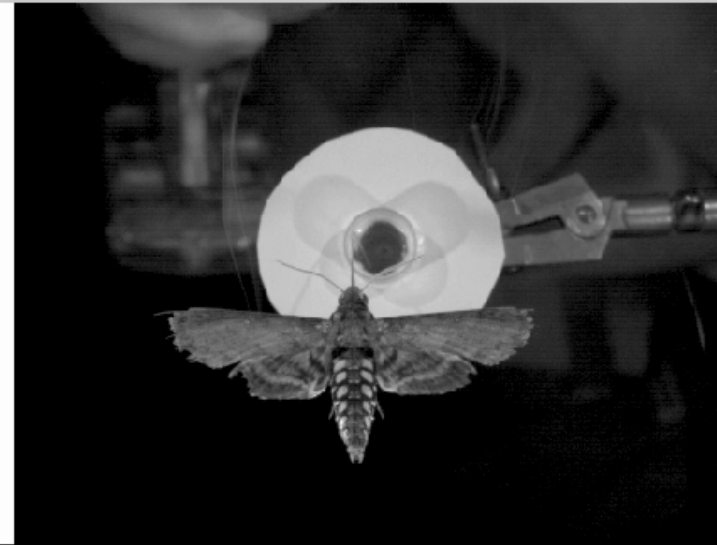
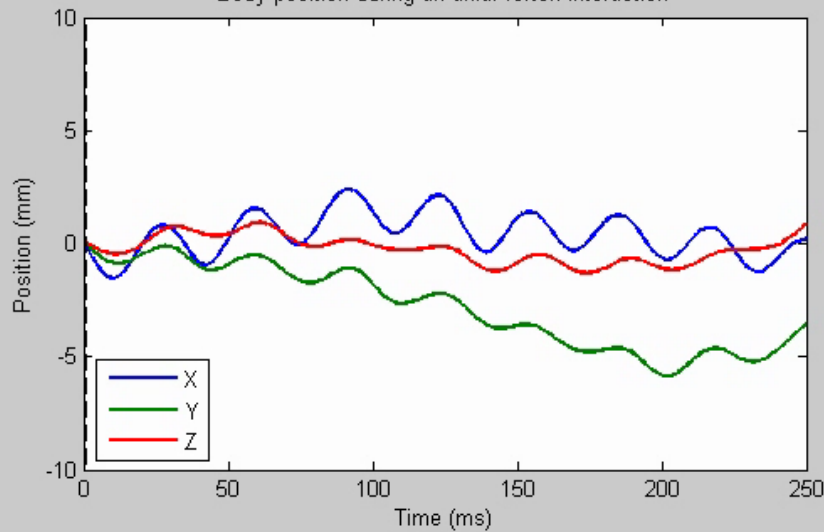


Liu et al.

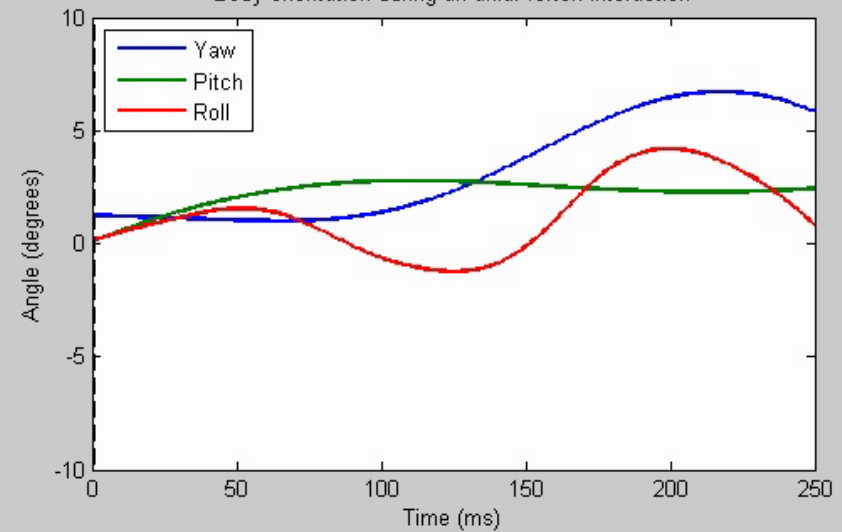
Vortex Ring Impingement Experiments



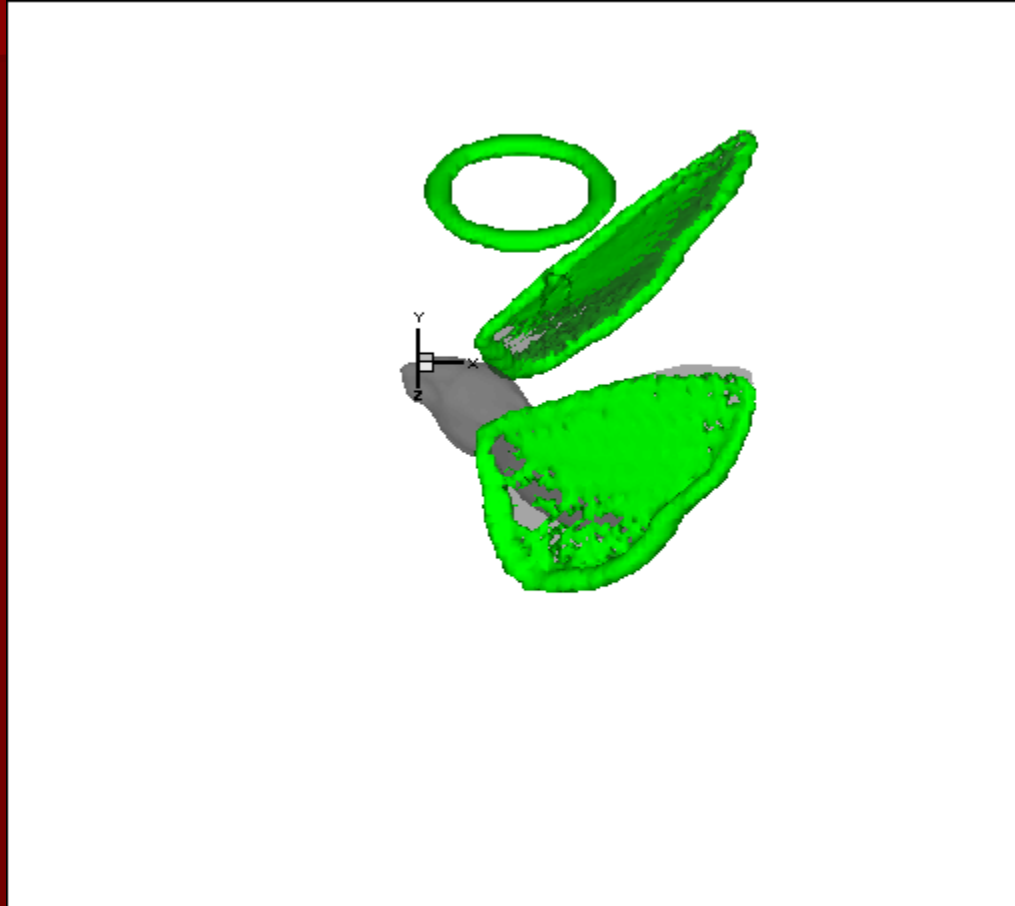
Body position during an axial vortex interaction



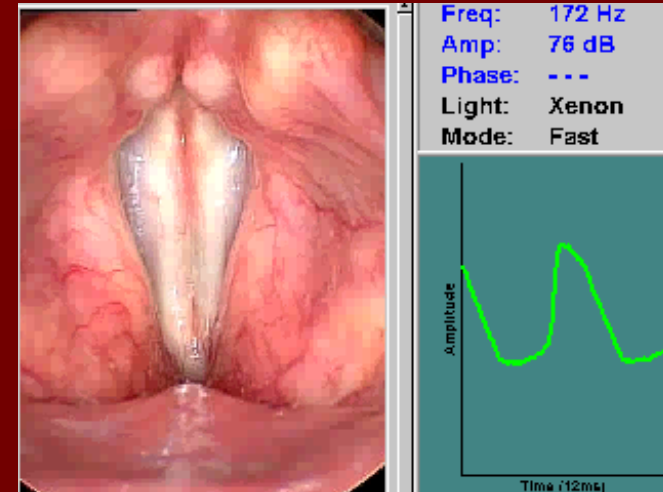
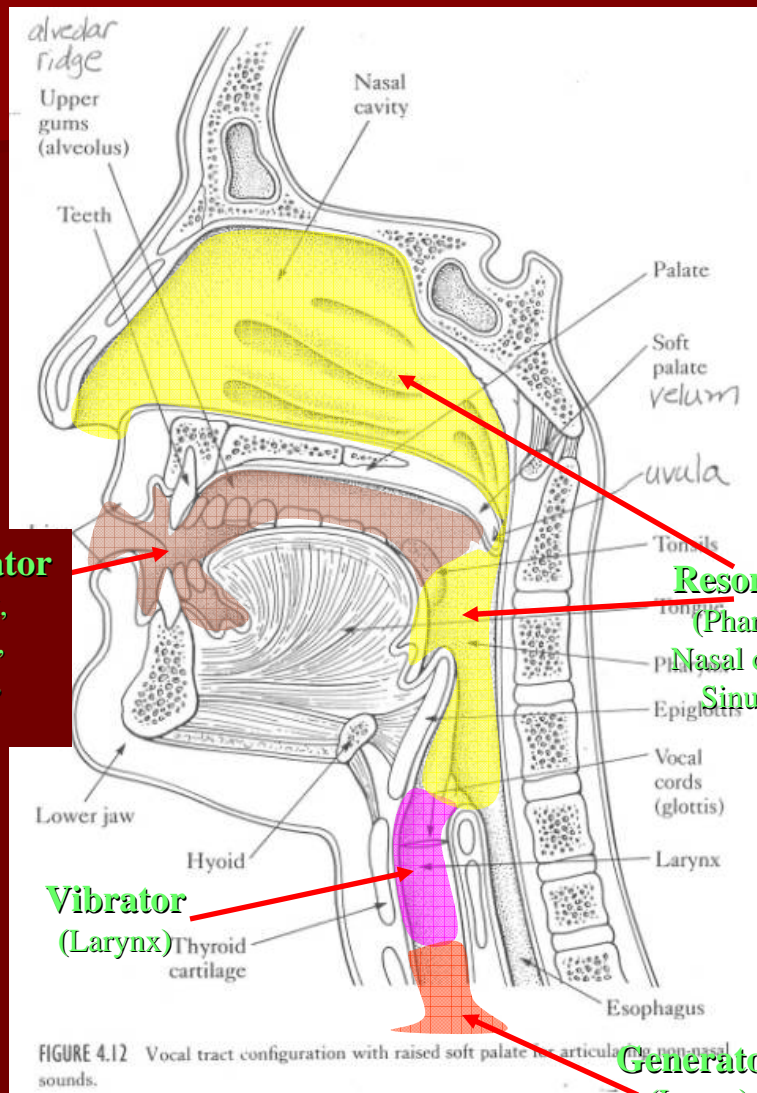
Body orientation during an axial vortex interaction



Vortex Ring Impingement: CFD



Biophysics of Phonation

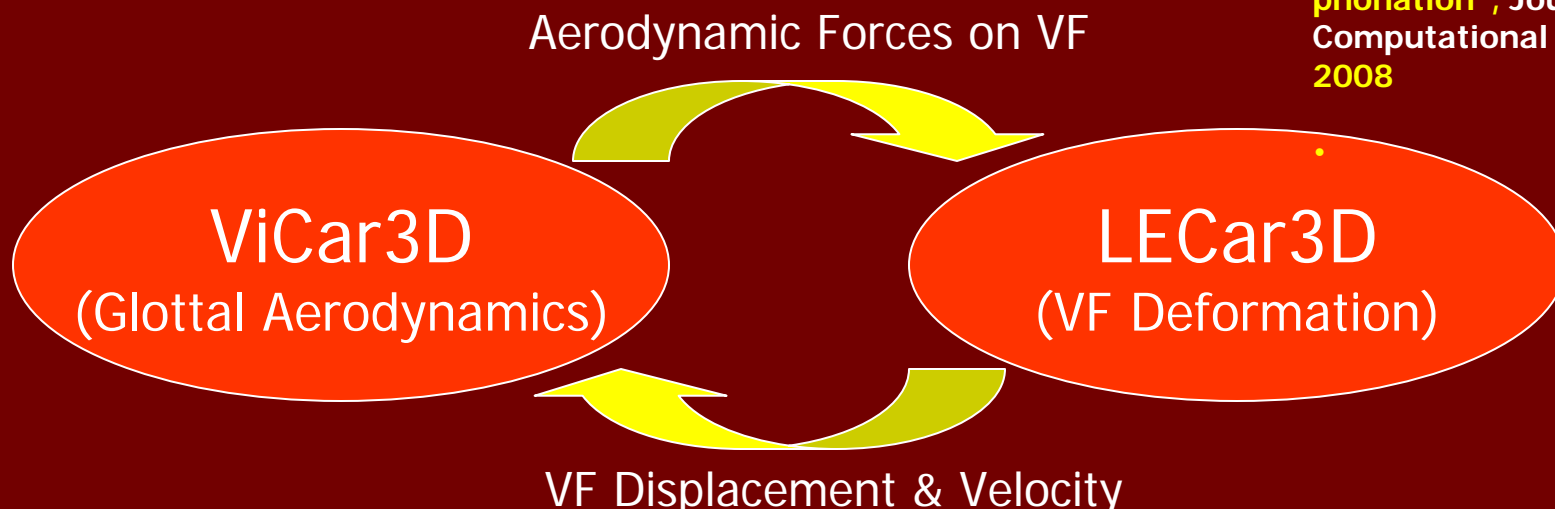


- NIH R01 grant focused on flow-structural interaction in larynx
- Understand the FSI mechanisms
- Apply knowledge to enhance laryngeal surgical procedures.

Modeling of Fluid-Tissue Interaction

- ViCar3D coupled to another solver that computes deformation of elastic structures
- Two approaches used for elastic structures
 - Finite-Element approach
 - Cartesian grid based approach (LECar3D)

• "An immersed-boundary method for flow-structure interaction in biological systems with application to phonation", Journal of Computational Physics, 2008



Structural Dynamics of VF

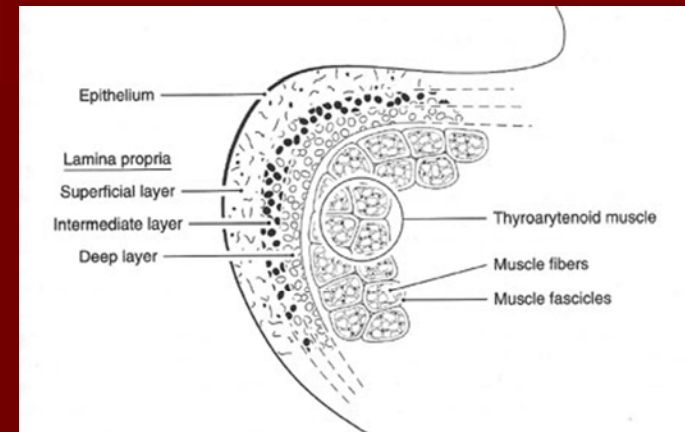
■ Governing equations

$$\frac{\partial \sigma_{ij}}{\partial x_j} + b_i = \rho \frac{\partial v_i}{\partial t} = \rho \frac{\partial^2 u_i}{\partial t^2}$$

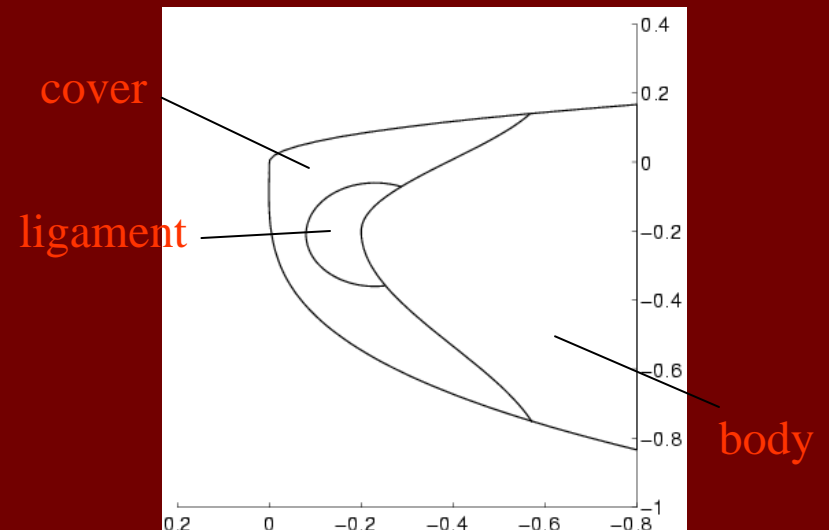
$$\sigma_{ij} = C_{ijmnp} e_{mn}$$

$$u_i = u_{b_i} \quad \sigma_{ij} n_j = T_i$$

- The tissue materials are assumed to be transversely isotropic.
- Material properties are obtained from experiments (e.g., Titze *et al* 2000).
- Multi-property, non-homogeneous structure



Schematic showing VF substructure



Model assumed in current study

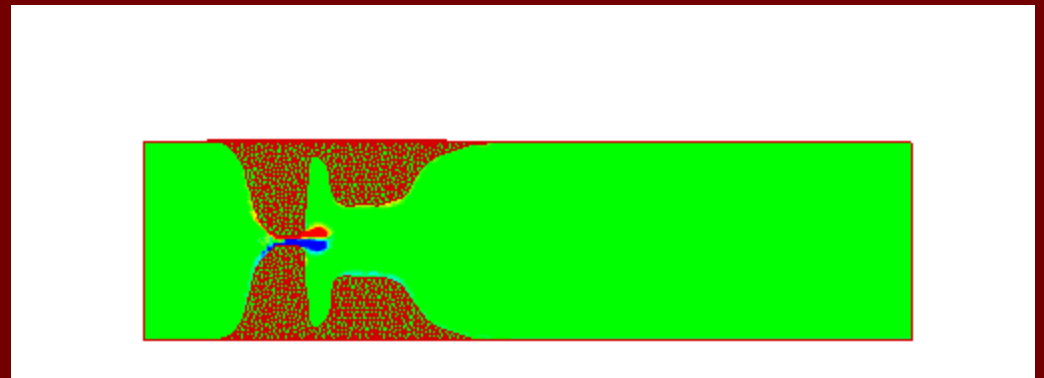
Flow-Induced Vibration (FEM)

■ Simulation Details

- 2D Simulation
- Geometry based notionally on CT scan of human larynx
- ViCar3D for air-flow
- Finite-Element for VF
- VF not fully adducted

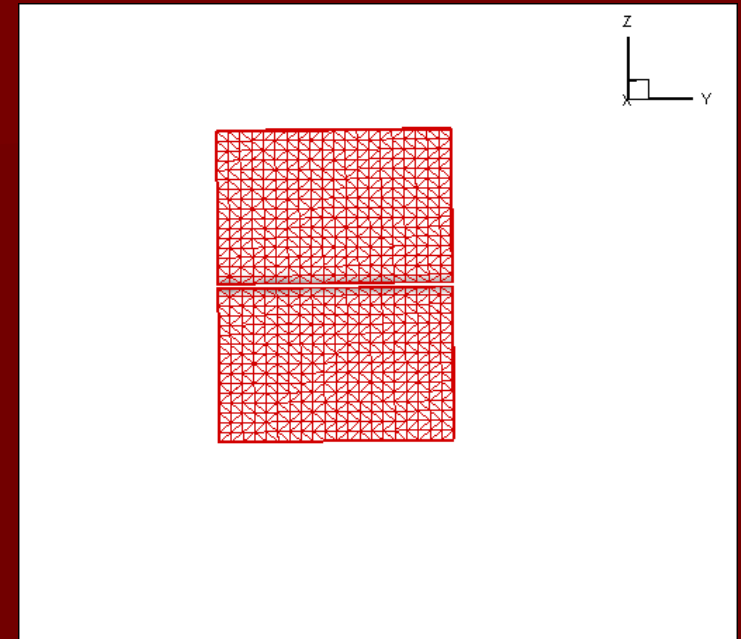
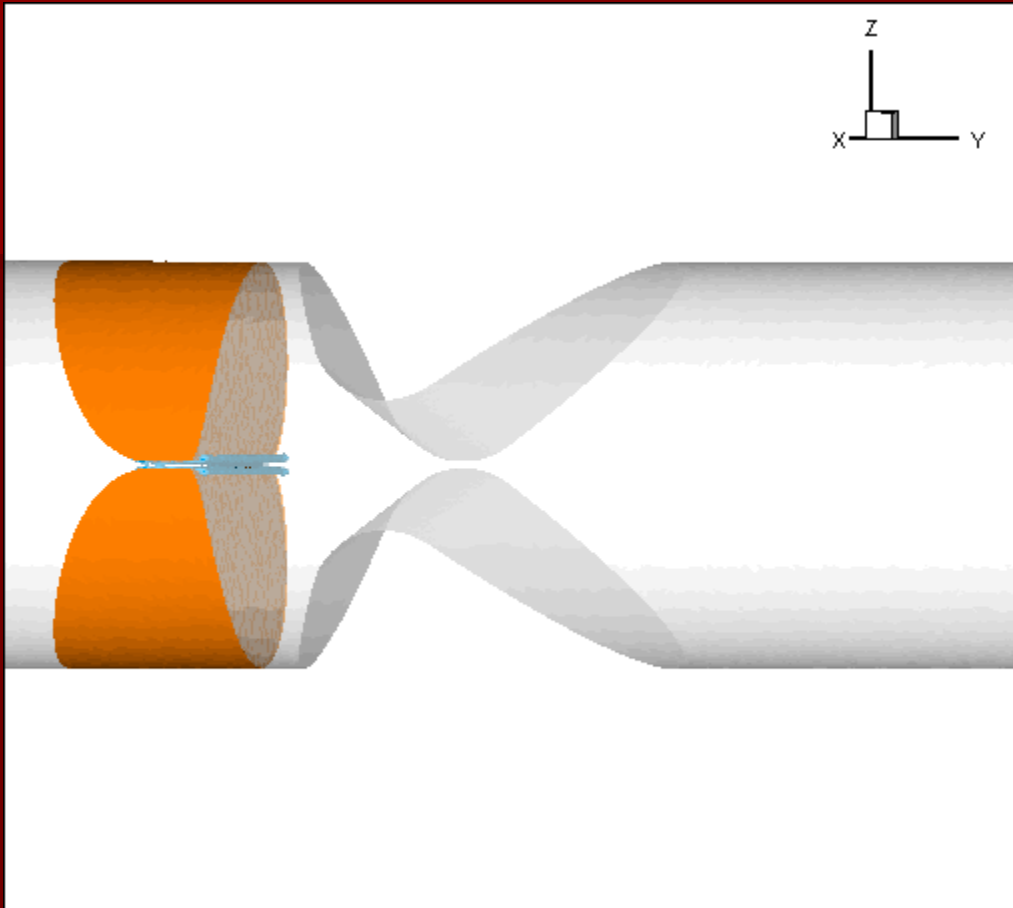
■ Observations

- Kelvin-Helmholtz vortices
- Bistable Jet
- Sustained vibrations of vocal folds.



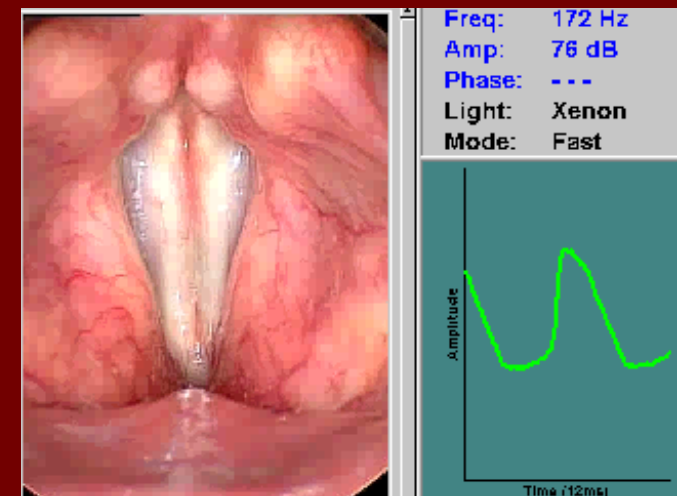
(400K points)

3D Vocal Fold Model



• Analysis of flow-structure interaction in the larynx during phonation using an immersed-boundary method; J. Acoust. Soc. Am. 126 2 , August 2009.

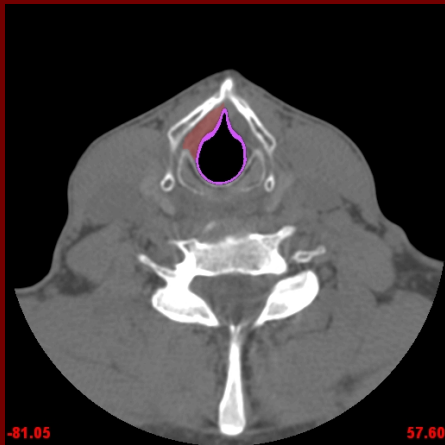
• Computational Study of the Effect of False Vocal Folds on Glottal Flow and Vocal Fold Vibration During Phonation," Annals of Biomedical Engineering, Vol. 37, No. 3 pp. 625-642 March 2009



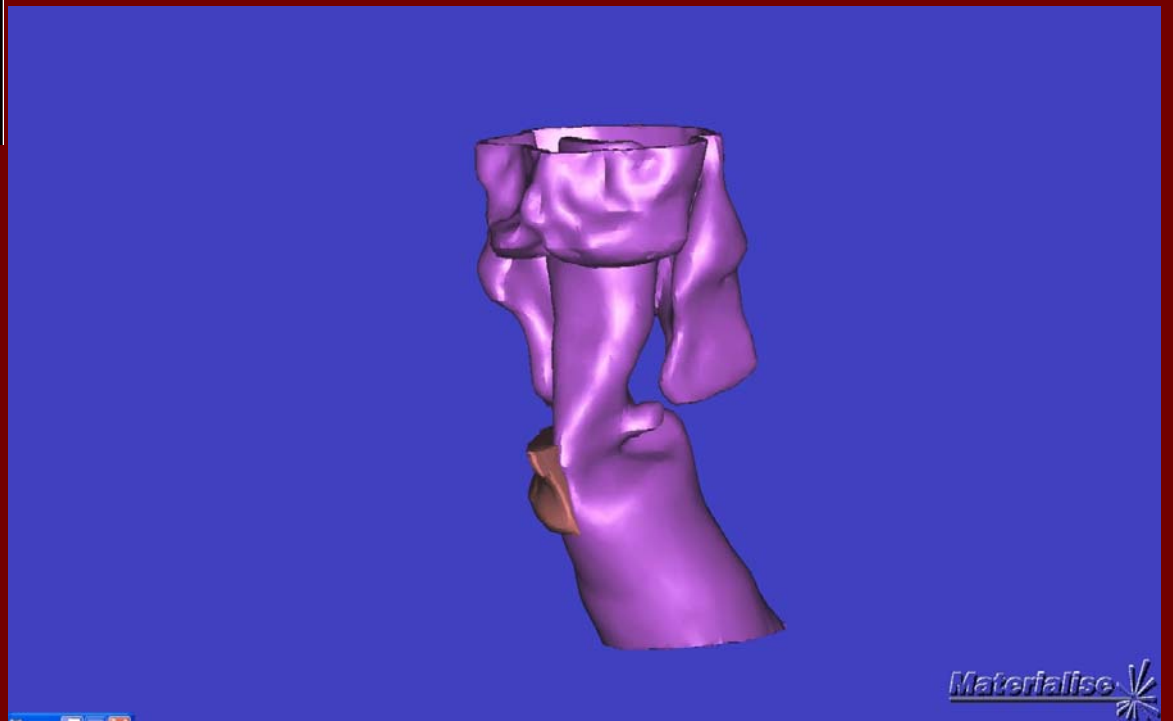
Towards Patient-Specific Models



Sagittal View



Axial View



Direct Computation of Low-Mach Number Sound Linearized Perturbed Compressible Equations (LPCE)

$$\rho(\vec{x}, t) = \rho_0 + \rho'(\vec{x}, t)$$

$$\vec{u}(\vec{x}, t) = \vec{U}(\vec{x}, t) + \vec{u}'(\vec{x}, t)$$

$$p(\vec{x}, t) = P(\vec{x}, t) + p'(\vec{x}, t)$$

Subtracting INS from CNS

Linearization and suppressing the generation and evolution of vortical component on the acoustic field.

$$\frac{\partial \rho'}{\partial t} + (\vec{U} \cdot \nabla) \rho' + \rho_0 (\nabla \cdot \vec{u}') = 0$$

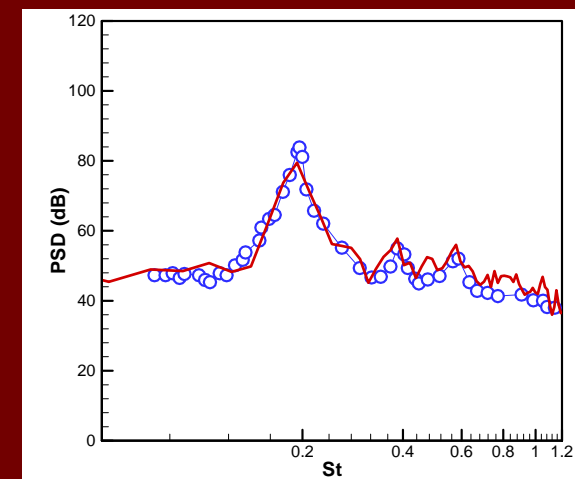
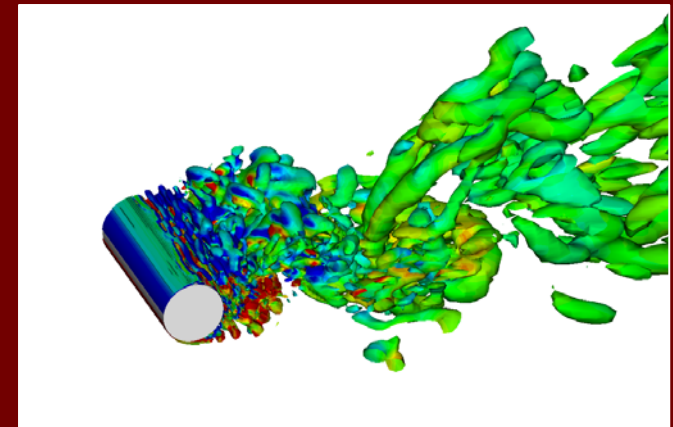
$$\frac{\partial \vec{u}'}{\partial t} + \nabla(\vec{u}' \cdot \vec{U}) + \frac{1}{\rho_0} \nabla p' = 0$$

$$\frac{\partial p'}{\partial t} + (\vec{U} \cdot \nabla) p' + \gamma P (\nabla \cdot \vec{u}') + (\vec{u}' \cdot \nabla) P = - \frac{DP}{Dt}$$

LPCE (Seo & Moon, JCP, 2006)

Need to use high (6th) order schemes to accurately model sound propagation

Noise generated by turbulent flow over a circular cylinder at $Re_D = 46000$, $M = 0.21$

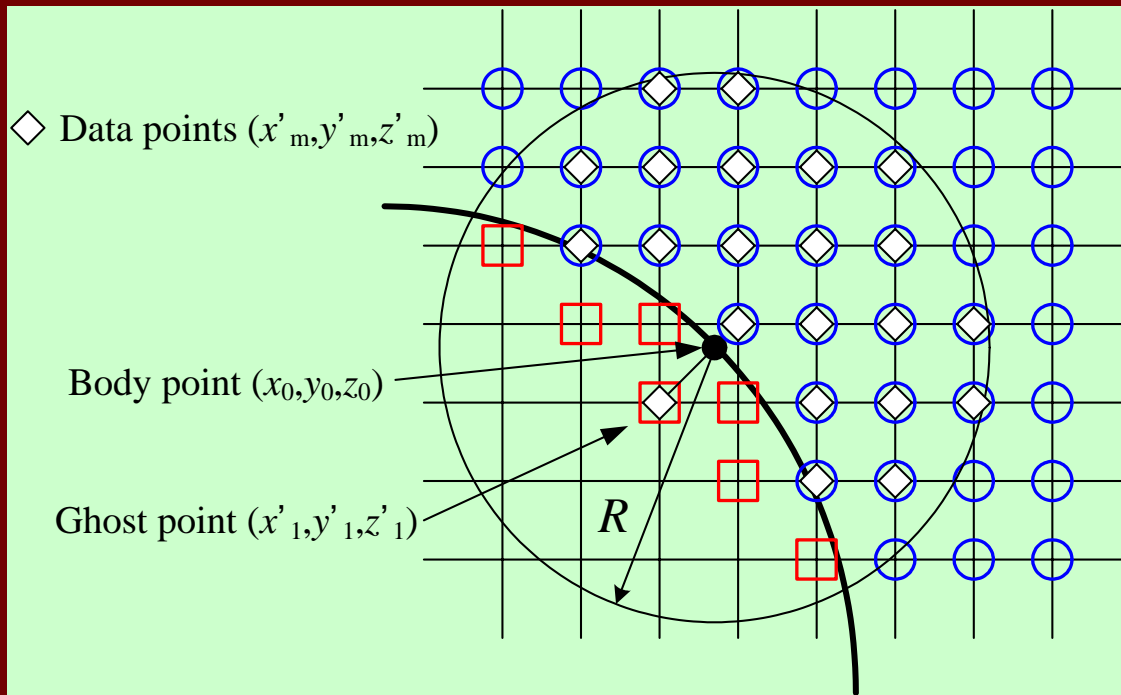


Immersed Boundary Method for LPCE (Approximating Polynomial Method)

(H. Luo et al.)

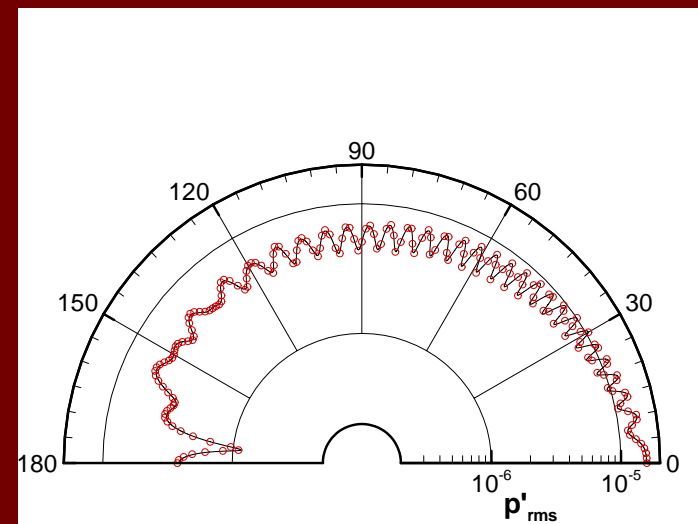
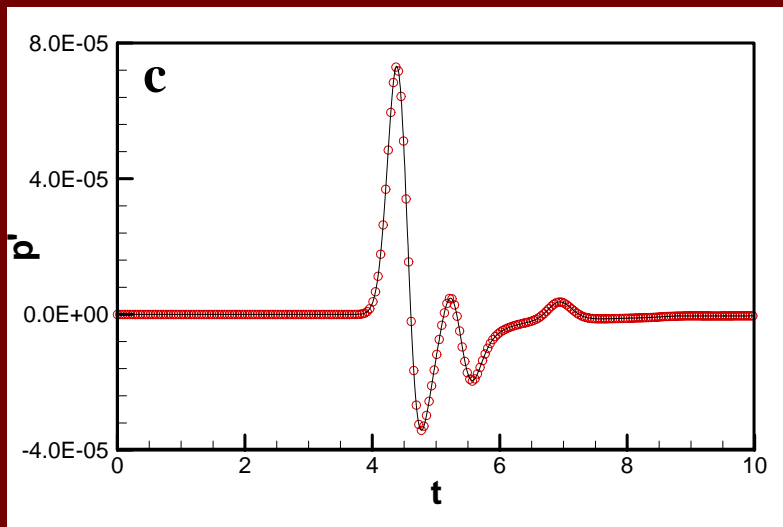
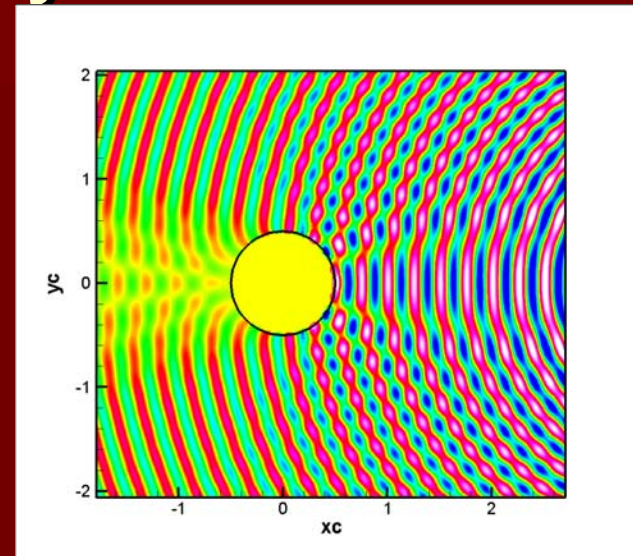
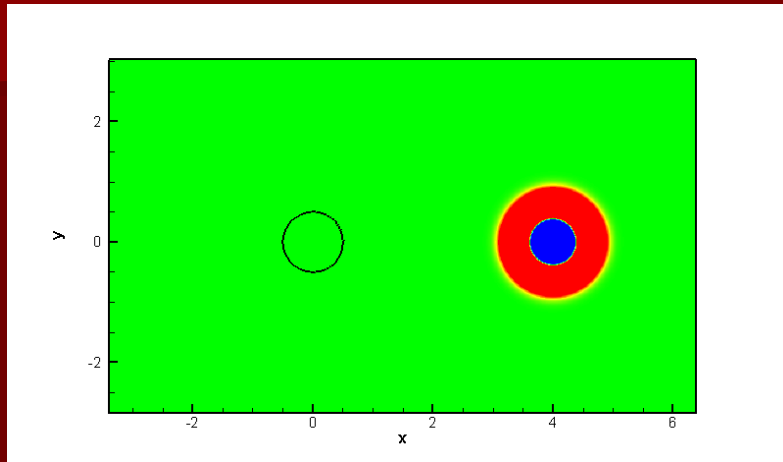
$$\phi(x', y', z') \approx \Phi(x', y', z') = \sum_{i=0}^N \sum_{j=0}^N \sum_{k=0}^N c_{ijk} (x')^i (y')^j (z')^k, \quad i + j + k \leq N$$

$$\varepsilon = \sum_{m=1}^M w_m^2 [\Phi(x'_m, y'_m, z'_m) - \phi(x'_m, y'_m, z'_m)]^2$$



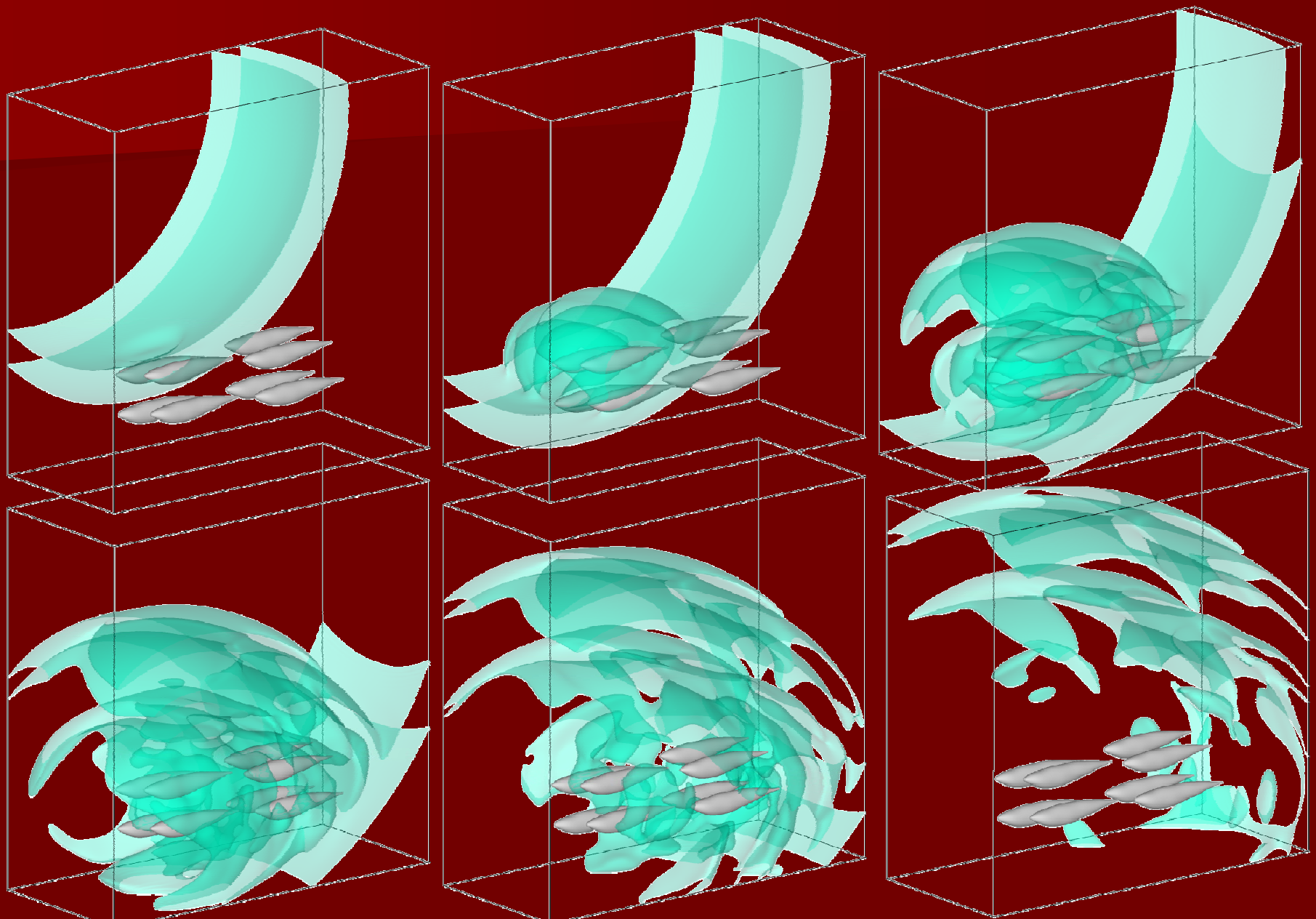
N	Number of coefficients	
	2D	3D
1	3	4
2	6	10
3	10	20
4	15	35

Benchmark: Sound scattering by a Circular Cylinder



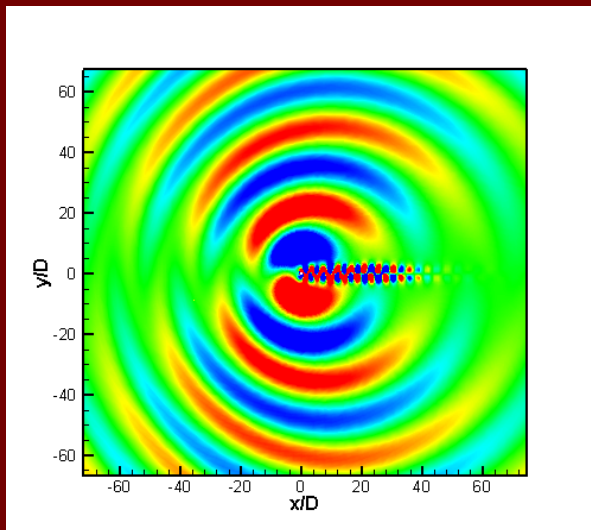
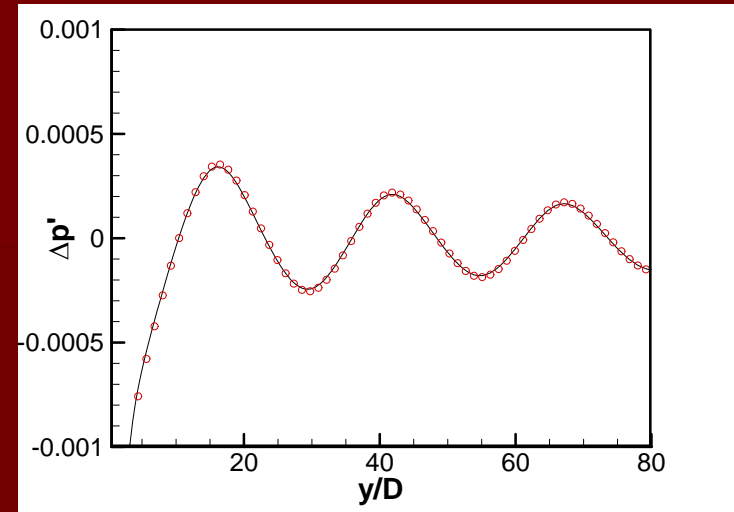
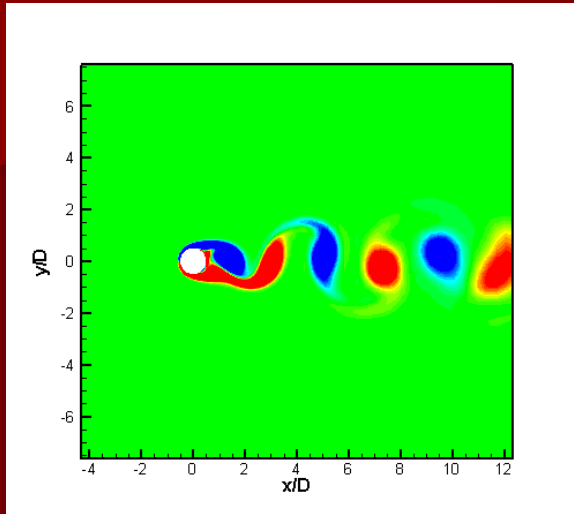
Directivity at $r=5$

Acoustic Scattering from Complex Geometries

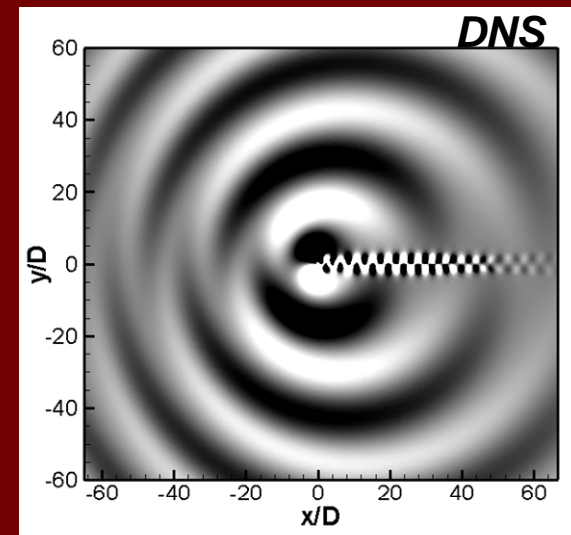


Comparison with DNS

ViCar3D

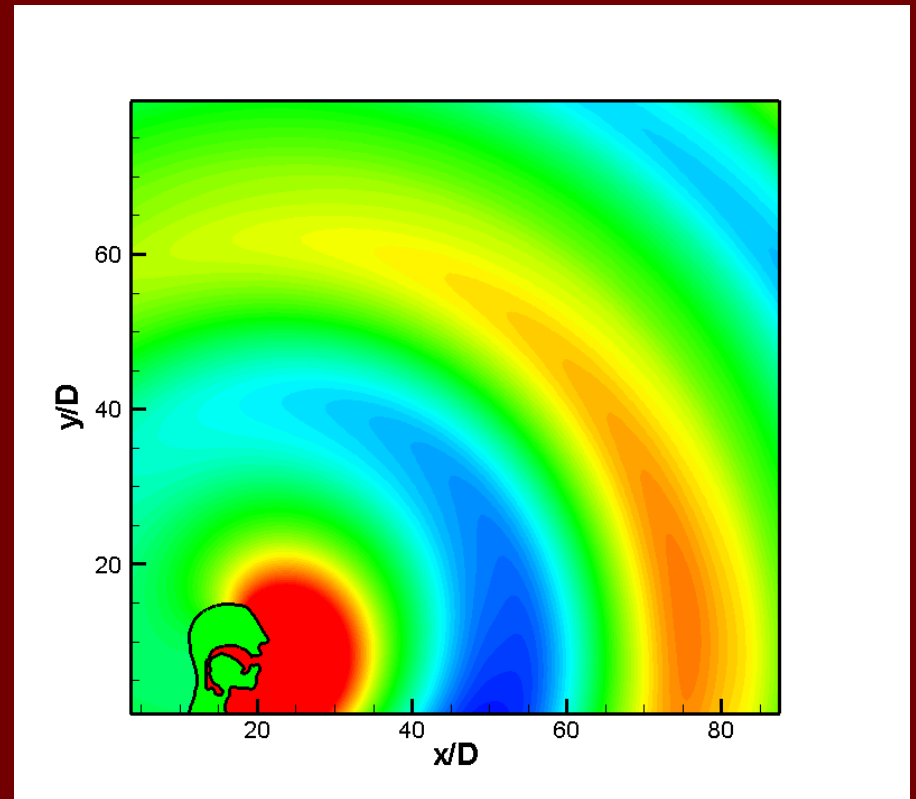
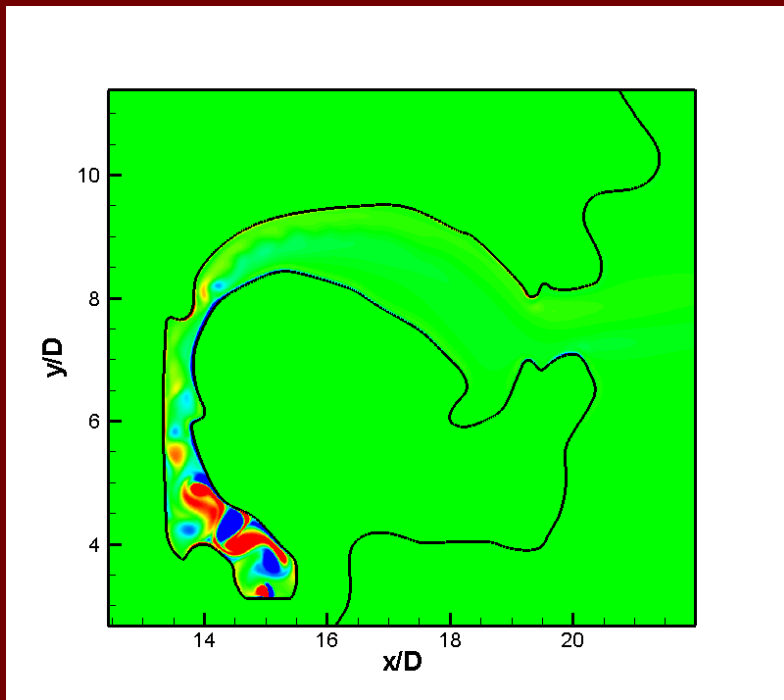
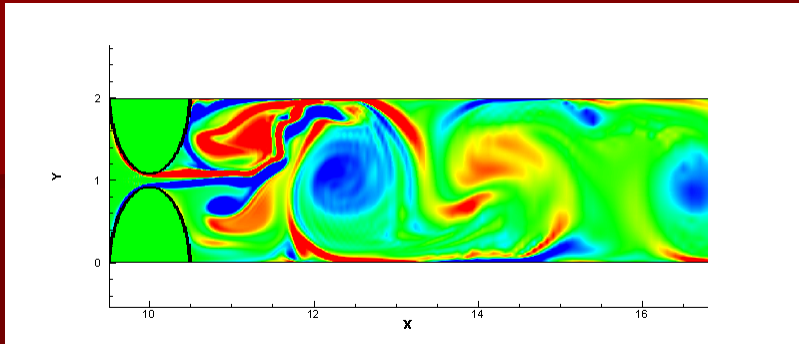


carLPCE

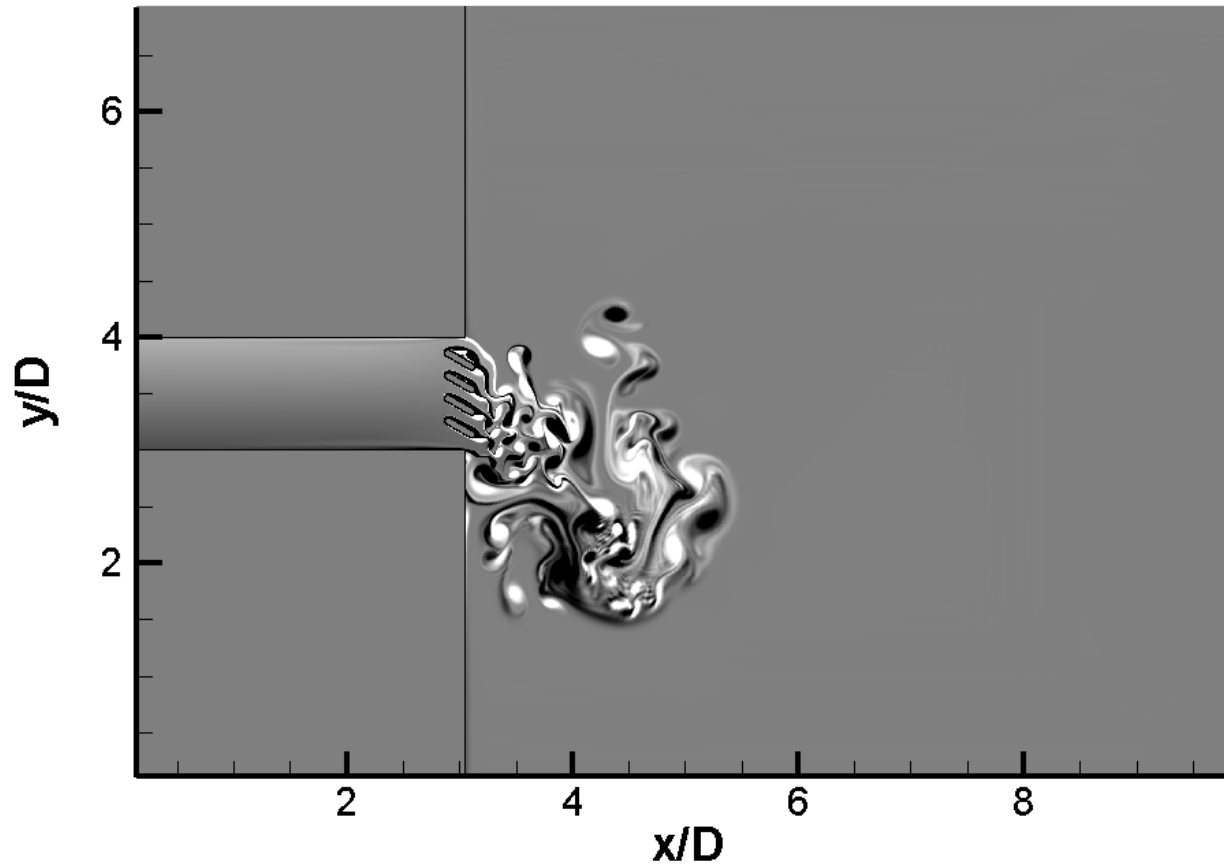


DNS : full compressible N-S
Eqs. on a body-fitted O-grid 34

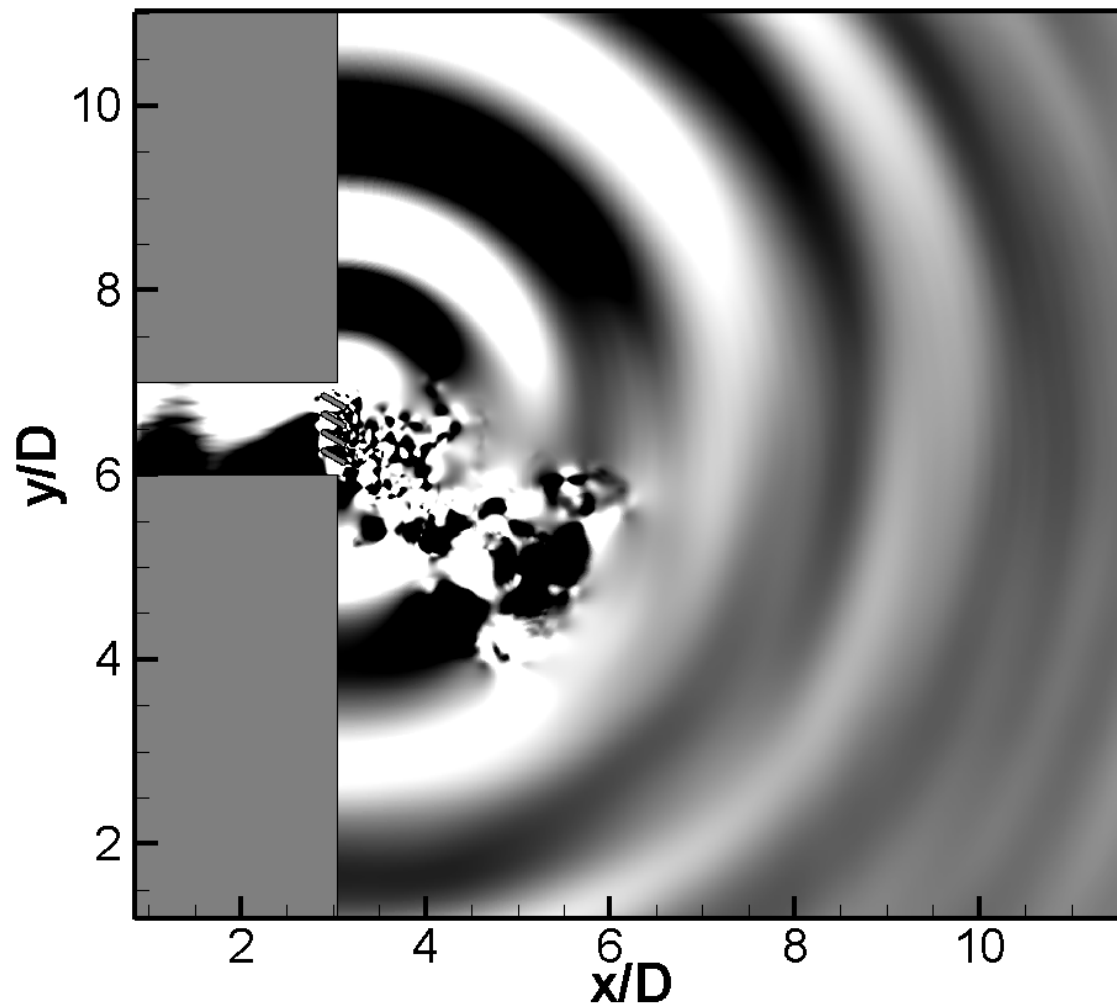
Phonation and Speech



Sound in Complex Configurations



Sound in Complex Configurations



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Questions?